## Engineering a Brighter Sudan

Bringing Sustainable Energy to the Theou Village School

# ELEC 492 Senior Design Project II Critical Design Review



A Design Report Submitted by

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#### **Abstract**

"Engineering a Brighter Sudan" involves bringing sustainable energy to a primary school in the remote village of Theou, Southern Sudan, where project member Mou Riiny was born. The project consists of specifying, designing, and building a power generation and storage system for the school as well as building a prototype system on campus at the University of San Diego. The prototype system provides electricity to a standard outlet at 230 Volts and 50 Hertz to conform to the standard in Sudan. This can power various loads including lights, laptops, and battery chargers.

We are using a 1.3 kW photovoltaic array on the roof of Loma Hall to provide power for the entire system. These solar panels are connected to a combiner box and wired to a mechanical skid in room 311 in Loma Hall. The mechanical skid houses all of the electrical equipment including a charge controller, inverter, battery bank, breaker box, and all the loads. The charge controller is used to regulate the power flow into our 48 Volt battery bank. The inverter converts the DC power from the solar panels and battery bank into standard AC power that is used to power the loads. The entire system uses a diagnostic program to monitor the system and show power flow in real time.

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#### 1. Context and Deliverables

Engineering a Brighter Sudan is a sustainable solution for bringing electricity to the Theou Village School in South Sudan. Electricity carries with it a world of benefits for rural communities, including the alleviation of poverty, reduction of illiteracy, and help for the local economy by providing opportunities for entrepreneurship. Our goal is to empower the people to obtain a higher level of education and independence, which will help a newly independent South Sudan prosper as a country.

To help achieve this goal, we have built a scaled prototype of the system on the University of San Diego campus. Because this project is a multidisciplinary effort, the system incorporates many aspects of both Mechanical and Electrical Engineering design. The Electrical Engineering component includes the wiring of all the electrical components, sizing of the system and wires, programming of all the equipment, and programming of the diagnostic system in LabVIEW. The Mechanical Engineering component includes designing and manufacturing of a skid to house the major electrical components of the system so they can be easily moved around Loma Hall.

The final design of the electrical system is modeled after the system that will be used in Sudan. For this reason, the system will provide electricity that is 230 Volts and 50 Hertz. This will be fed into a type D outlet which is the standard outlet for Sudan. This outlet will be used to power various loads including lights, laptops, and a battery charger.

A large portion of the electrical design comes from sizing the wires and the circuit breakers for safety. Each wire used in the system must be sized for the correct amperage and must be protected by a breaker to ensure that this current is not exceeded. In addition to this, we have incorporated ground fault protectors in the AC and DC side of the system to protect people from the electrical hazards inherent in a system like this.

We have also created a program to read data from the inverter, charge controller, and FlexNET DC and analyze it in LabVIEW. This program has two primary purposes: first to monitor the power flow of the system in real-time, and second to diagnose when the system is not functioning correctly. This is done by comparing the real time data to historic data that is also logged using the LabVIEW program.

Finally, there is the mechanical component of our prototype design. This consists of the design and fabrication of a skid which carries many of the electrical components of the system. This skid houses the inverter, charge controller, batteries, breaker box, and all the loads that our system will power. The skid is mounted on wheels so that we can move our system around Loma Hall with ease.

The final system is located both on the roof and in room 311 in Loma Hall. The solar panels and combiner box are on the roof while the skid and all the other electrical components are in Loma 311. The system in room 311 will be on display for the campus community.

#### 2. Design Analysis and Results

Our design analysis and results can be broken down into three subsections. First, there is a description of the overall prototype system. Second, there is a section detailing all of the subsystems. Finally, there is a section describing our test plan for the system.

#### 2.1. System Description

The block diagram for the final prototype system can be seen in Figure 1 below.

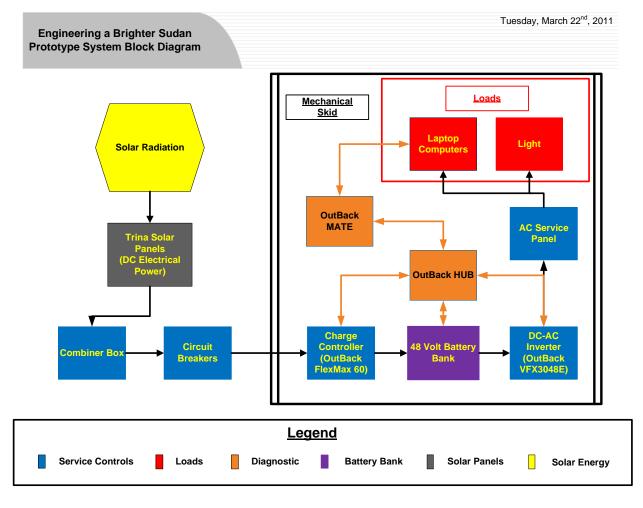


Figure 1: System Block Diagram

The block diagram can be separated into three major categories. First, the flow of power from the solar panels to the loads is represented by the black arrows. Second, the flow of information from the different electrical components to the diagnostic is represented by the orange arrows. Finally, the box on the right illustrates which electrical components are mounted on the mechanical skid.

A better representation of our final prototype system can be seen in the system layout diagram in Figure 2 on the next page. Note, scaled drawings of the skid and electrical components can be found in Appendix B.3. and Appendix B.4.

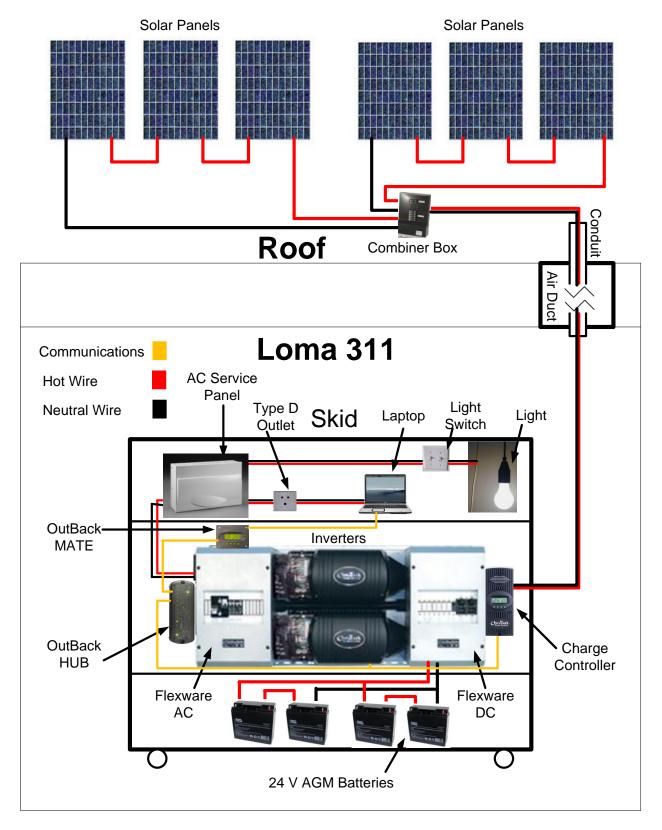


Figure 2: System Layout Diagram

Figure 2 shows all of the components that are being used in the final prototype system. The solar panels and the combiner box are located on the roof of Loma Hall while the rest of the electrical equipment and the mechanical skid are housed in Loma 311. The black lines in the figure represent neutral wires, the red lines represent positive wires, and the orange lines represent the flow of information through the system.

The final prototype system has two sets of three solar panels connected in parallel by a combiner box on the roof of Loma Hall. The combiner box houses 15 amp circuit breakers to ensure that none of the solar panel circuits exceed the current rating for the wires that are being used. The two strings of solar panels can be treated as current sources when they are connected together.

The output of the combiner box is connected to the equipment in Loma 311 using existing wires from the old wind turbine on the roof. These wires are housed in conduits and routed through an air duct which leads to Loma 311. The wires are connected to a charge controller which regulates the solar panel voltage and current to charge a 48 Volt battery bank. Power from the charge controller and battery bank is sent to the inverter which converts the 48 Volt DC input to AC electricity at 230 Volts and 50 Hertz which is used by the loads.

This output is sent to the AC service panel which houses the circuit breakers for each individual circuit. One circuit is wired to a light switch which is used to turn a light on and off. The other circuit is used to power a type D outlet which can power various loads. Both of these circuits are wired to ground fault circuit interrupter (GFCI) breakers to add an element of safety for people using the equipment. An outlet adaptor and voltage transformer are being utilized to accommodate loads that run on different voltage standards.

Data from the inverter, charge controller, and batteries are sent to a laptop using the OutBack HUB and MATE. This includes information such as voltage, current, battery charge level, equipment mode, and much more. This information is uploaded to a laptop using an RS 232 to USB cable. A LabVIEW program is used to read and analyze this data in real time. The program has two primary purposes. First, it shows the power flow through the entire system using a user interface that makes it easy to monitor what is going on with the system. Second, there is a diagnostic program that is running in the background which monitors the system to find potential system failures. The program also allows the user to send basic commands to control the inverter.

All of the electrical equipment that is used in Loma 311 is housed in a mechanical skid. The first level of the skid holds four 24 Volt batteries connected in both parallel and series. The second level houses the FlexPower unit which includes the charge controller, inverter, DC wiring box, and AC wiring box. The third level of the skid houses the AC Service Panel and all of the loads that our system is powering. The skid is mounted on wheels and is designed to easily transport all the electrical equipment.

#### 2.2. Subsystem Descriptions

The responsibilities for our project can be divided into four parts. Emmett Perl is in charge of the power delivery subsystem, Mou Riiny is in charge of the safety subsystem, Michael Rios is in charge of the diagnostic subsystem, and Enrique Rayon is in charge of the mechanical subsystem.

#### Power Delivery Subsystem

Subsystem Lead Personnel: Emmett Perl Subsystem Support Personnel: Mou Riiny

#### **Design Specifications**

The design specifications for the power delivery subsystem are shown below in Table 1:

**Table 1: Design Specifications for Power Delivery Subsystem** 

Specification	Design	Plan for Measurements & Validation
Standard Outlet and light switch must be wired to accept 230 Volt, 50 Hertz input power	Standard type D wall outlet and light sensitive switch have been bought and wired with three wires: hot, neutral, and ground	Digital multimeter will be used to assure that wiring and output power from outlet and light switch are correct
Battery bank must be set up to provide 48 Volt DC input to inverter	There are four 24 Volt batteries connected in series and parallel to provide 48 volts to the inverter	Digital multimeter will test the voltage of the batteries to assure that they are set up correctly
Inverter must be programmed for 48 Volt input power and 230 Volt, 50 Hertz output power	An OutBack VFX3048E is being used, which is designed for the correct input and output voltages	Digital multimeter will test the inputs and outputs to the inverter
Charge Controller must be programmed to charge a 48 Volt battery bank	Charge Controller is configured to automatically convert the solar panel voltage to 48 Volts	Digital multimeter will test the voltage at the input and output of the charge controller
Power flow program must be designed to read data from the inverter, charge controller, and battery bank	LabVIEW program is designed to read data from the OutBack MATE and sort it into an array	Values will be compared to specifications for each piece of equipment
Flow diagram must be designed in LabVIEW Front Panel	The program is designed to show how power is flowing through the system (voltage, amperage, etc.)	This front panel be integrated into the power flow program
Program must log historic performance of the system and show it on the front panel	Data from the power flow program will be stored in a comma separated variable file that can be accessed by the program	Visual inspection of data and debugging will be used to perfect the reading and writing of data to and from a text file

The design for the power delivery subsystem meets all of the specifications from Table 1. The design is centered around the inverter, which is the central component in the power delivery subsystem. Since the inverter requires a 48 Volt DC input and a 230 Volt, 50 Hertz AC output, all of the electrical equipment must conform to these power levels. To accommodate the DC input, the charge controller has been programmed and the battery bank has been wired to provide 48 Volts to the inverter. All of the AC circuit breakers are designed for 230 Volt, 50 Hertz power and a type D outlet and switch have been wired to the AC service panel.

The power flow program was designed to read data from the inverter, charge controller, and FlexNET DC in real time. This data is placed into an array and sorted so that it can be shown in a meaningful manner on the front panel of the LabVIEW program. This allows us to extract useful data such as battery level, solar panel voltage, output AC current, and the mode for each piece of equipment. The front panel of this program is designed to show all of this data in a user friendly way that can be easily interpreted by people unfamiliar with the system. The program also saves the data into a large array and writes it to a text file after a specified amount of time has passed. This text file can be read back into the program to show the historic performance of the system.

#### Subsystem Current Status

This subsystem is currently in the testing stage. All of the necessary electrical components have arrived and are hooked up in the system. This includes solar panels, a combiner box, charge controller, battery bank, inverter, AC service panel, and all the necessary wires. Figure 3 shows

many of the components that are used in the power delivery subsystem.

The power delivery subsystem consists of six 230 watt Trina solar panels, an OutBack combiner box, an OutBack Flexmax 60 charge controller, a 48 Volt battery bank, an OutBack VFX3048E inverter, and an AC service panel which connects to all of the loads.

The entire system is currently connected and running. We are testing the voltages throughout using a digital multimeter and are starting to characterize the



Figure 3: Prototype System on the Roof of Loma Hall

system using a power flow program. When this program is developed and debugged, it will be possible to monitor the functionality of the power delivery subsystem through LabVIEW alone. Once historic data is logged for the system, it will be possible to integrate the power flow data into the diagnostic program that is currently being developed.

The second part of the power delivery subsystem is the design of a power flow program. This program reads in data from the charge controller, inverter, and FlexNET DC. It then sorts this data into an array and displays it on the front panel. Some of the data that it displays includes solar panel voltage, solar panel current, charger mode, battery charge level, and solar power

output. The flowchart for the power flow program is shown in Appendix B.1. The commented LabVIEW code for the current power flow program is shown below in Figure 4.

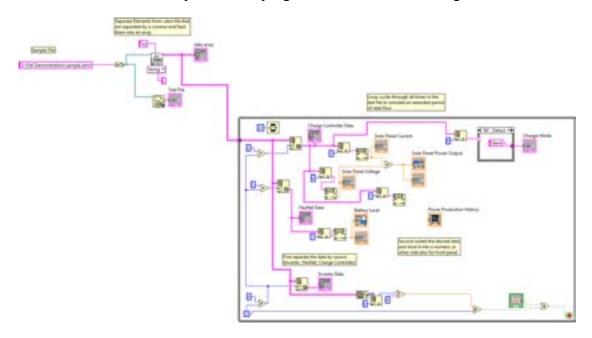
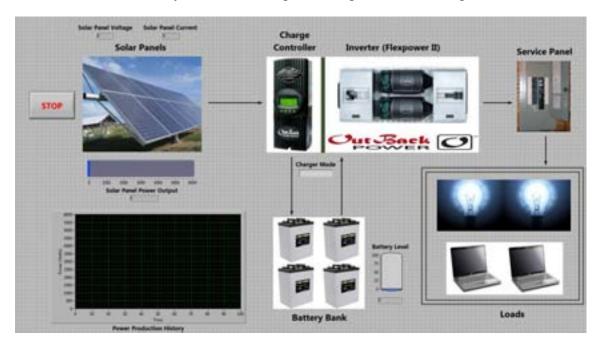


Figure 4: Power Flow Block Diagram

The data from the system is displayed on the front panel of LabVIEW. This is designed to show the layout of the system and to show the how the power is flowing through the major components. It also graphs the historic data and gives the user the option of looking at power flow for each individual subsystem. The front panel design is shown in Figure 5 below:



**Figure 5: Power Flow Front Panel** 

Data from the power flow program is stored in a text file which can be read back into LabVIEW. This data is used for two purposes: to show the power production history and for the diagnostic subsystem.

The power flow program is currently in the debugging stage. While it is working with the system, there are many improvements that can be made. In particular, the reading and writing of the data needs to be perfected. Debugging this program will be the primary objective for the remainder of the semester.

#### Electrical Safety Subsystem

Subsystem Lead Personnel: Mou Riiny Subsystem Support Personnel: Emmett Perl

#### **Design Specifications**

All the design specifications for the electrical safety subsystem can be seen in Table 2 below:

**Table 2: Design Specifications for Electrical Safety Subsystem** 

Specification	Design	Plan for Measurements & Validation
All wires must be designed with current carrying capacity that meets or exceeds the NEC code	All wires from the DC side of the system are sized to carry up to 35 Amps (AWG #10). All wires from AC side are sized to carry up to 115 Amps (AWG #2).	Digitsal multimeter will be used to measure current in wire and will be compared to the maximum current the wire can carry
System must have disconnect between array and charge controller	(2) 15 Amp DC breakers are used to protect the wire in the array circuits	Breakers between array and charge controller will be shut down and system evaluated to make sure that the power is cut off
Ground Fault Protection must be used where outlets are present	(4) Ground fault protected AC breakers used to wire all outlets.	The test button of the GFCI breakers will be pressed to make sure it is functioning properly
System must have disconnect between charge controller and batteries	(4) 80 Amp DC breakers used between charge controller and batteries	These breakers will be shut down and the system evaluated to ensure that power from charge controller is cut off completely
System must have disconnect between batteries and inverters	(2) 80 Amp DC breakers used between batteries and the inverter	These breakers will be shut down and the system evaluated to ensure that power from the batteries is cut off completely
System must be properly grounded	System is properly grounded with a TBB-green and AWG #8 wire.	System will be inspected carefully by a professional to make sure all grounding is done correctly
Metallic equipment must be grounded or protected by conduit	All solor moduls and metalic equipment that come in contact with wires are properly grounded with TBB- green and AWG #8.	System will be inspected carefully by a professional to make sure all grounding is done correctly
Loads must be protected from overcurrent	All loads are protected with (2) surge protectors connected to the output end of each inverter	A professional will inspect the system to make sure the surge protector is connected properly and will protect the equipment it is intended to
A clear, effective operation and maintenance manual must be provided	Operation and maintenance manual written with text and pictures for clarity	Manual will be given to different people and they will evaluate it for clarity and effectiveness
A system troubleshooting manual must be provided	A comprehensive troubleshooting manual written with emphasis on the system's most likely points of failure	Troubleshooting will be done by turning off power to certain components and people unfamiliar with the system will be asked to see if they find the manual useful in solving these problems

All wires have been designed to meet national safety standards. This means that the wire sizing of the entire system has met or exceeded the standards necessary for the National Electric Code (NEC). The system has also been wired with proper wire sizes to minimize losses and to prevent the wires from overheating. Wire gauge selection was based on several factors including the wire carrying capacity (ampacity), temperature, location covering, insulation, and outer jacket type.

Based on the wire sizing calculations shown in Table 6 in Appendix B.3, the wire connecting the solar panel array to the charge controller and inverter must be able to carry at least 25.97 Amps and the wire from the storage system to the inverter must be able to handle a current of 104.17 Amps. Taking this into account, the gauge selections were AWG #10 (American Wire Gauge) from the array to the charge controller, AWG #2/0 from storage system to the inverter, and AWG #2 from the inverter to the AC Service Panel. All of the wires are copper. All of the calculations, tables, and figures are shown in Appendix B.3.

Each piece of equipment in a PV system must be able to be disconnected from all sources of power (NEC 690.15). The NEC also requires that every ungrounded conductor be protected by an overcurrent device (NEC 240.20). This provides multiple levels of protection for the vital electrical components of the Inverter in the event of an electrical surge or nearby lightning strike. The wiring diagram in Figure 6 shows all the breakers, surge protectors, and GFCI's required to adequately protect the system and meet all the design requirements.

#### Subsystem Current Status

The sizing and gauge selection of the wires for the entire system has been completed. This was done according to the NEC code. All wires for the demonstration were ordered and have been received. There are many circuit breakers in the system and selecting the correct sizes to meet the design specifications presented a challenge because they must all match the wires that will be used both for the prototype system and for the final system in Sudan. At this point all the circuit breakers required for the demonstration have been ordered and received. In addition to this, two surge protectors were also sized to protect the system and have been wired to the OutBack inverters.

Grounding the system was one of the biggest challenges because it is hard to make sure that everything is grounded and because there are many dangers that can occur when a system is grounded incorrectly. A professional engineer has looked over our system to confirm that the grounding and wiring of the system is correct.

The circuit breakers for the system are located in the combiner box, the Flexware DC enclosure, the Flexware AC enclosure, and the AC service panel. The combiner box has two 15 Amp circuit breakers to protect the solar panel circuits. The Flexware DC has two 80 Amp circuit breakers and a GFCI breaker to protect the circuits connecting the charge controller to the battery bank and solar panels. The Flexware AC has six 30 Amp circuit breakers to protect the inverter output circuit. The AC service panel has two GFCI breakers to protect the circuits that are connecting

the loads. An operation and maintenance manual has been developed to categorize the system and identify all the safety hazards associated with it. This is shown in Appendix B.6.

A wiring diagram for the entire prototype system is shown below in Figure 6:

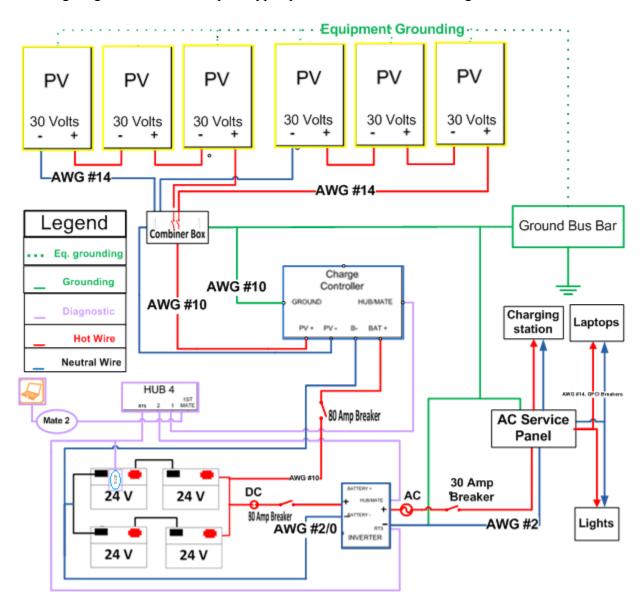


Figure 6: System Wiring Diagram

Figure 6 shows all of the intricacies of the system wiring. This diagram has a lot of information including the gauge of each wire group, the grounding scheme, the location all of the circuit breakers, the location of the diagnostic cables, the location of the hot and neutral wires, and the location of all the major electrical components. All of the major electrical components and the neutral wire must be connected to ground. The legend on the left side of the diagram shows what each color in the diagram represents.

Subsystem Lead Personnel: Michael Rios Subsystem Support Personnel: Emmett Perl

#### Design Specifications

All the design specifications for the diagnostic subsystem can be seen in Table 3 below:

**Table 3: Design Specifications for Diagnostic Subsystem** 

Specification	Design
Communicate with the system via the OutBack MATE.	Use LabVIEW to pull raw data from the MATE
Manipulate raw data from MATE	Sort through the raw data to extract the important information
Provide instructions for system debugging in the presence of a system error	Use LabVIEW to create "cases" that will notify the user of system errors

The diagnostic subsystem is a critical component to the overall system because it helps assure that the system is functioning properly. The main purpose of the diagnostic is to take the raw data from the major electrical components and upload them to a laptop. This is done by communicating with the OutBack MATE using the serial communication protocol in LabVIEW. We are able to extract the useful information from the raw data which allows us to display it to the user. It is necessary to manipulate the raw data in a way that will extract the important information.

The second major component to the diagnostic system is the ability to communicate errors to the user. When an error occurs, the diagnostic program will create a popup which will provide instructions for debugging the system. This allows the user to physically see when the system is not functioning correctly. The user can then follow the error window's instructions or refer to the system manual to correct the error. The goal of the diagnostic is to make the debugging process as simple as possible.

#### Subsystem Current Status

The status of the diagnostic subsystem can be summarized by the serial communication configurations, raw data sorting, and error windows.

The serial communication configuration was necessary to be able to pull raw data from the MATE into LabVIEW. The process began with the specifications defined in the MATE Serial Communications Guide. Information from the charge controller, FlexNet DC, and inverter is combined through the HUB and sent to the MATE. An isolated RS-232 port allows for all the

data from the MATE to be sent to a computer. An RS-232 to USB cable is used to facilitate the data flow from the MATE to LabVIEW.

The next step was the get LabVIEW to display the string of raw data and provide real time data gathering. The serial communication program configures all the correct settings on the PC:

19200 baud rate, 8 bits, no parity, and 1 stop bit. In addition to configuring all of these settings, it was required that the DTR (pin 4) be driven high and that RTS (pin 7) be driven low in order to power the port. Once the DTR and RTS pins were set to the correct values, we were able to extract live raw data from the MATE. The raw data feed can be seen in Figure 7.

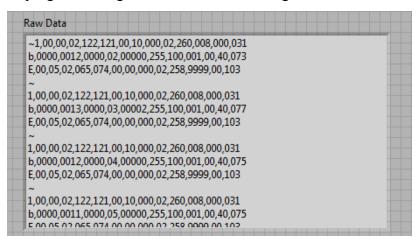


Figure 7: Raw Data Feed

The next step was to sort this data into meaningful information about the system. By using the byte definitions from the Serial Communications Guide, we were able to sort the raw data into the appropriate fields. For example, the byte definitions for the inverter can be seen in Figure 8:

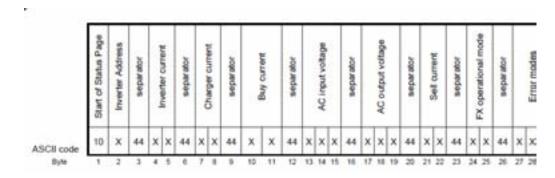
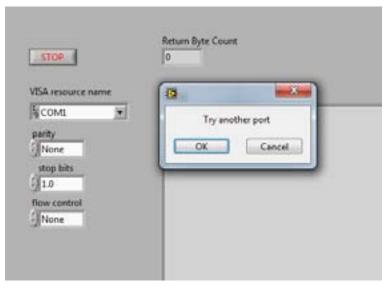


Figure 8: Byte Definition Map for Inverter

The next step is to separate the data according to the appropriate electrical component, i.e. charge controller, inverter, FlexNET DC. Once this is done, it can be broken down further based on the different byte definitions. For example, the AC output voltage of the inverter can be extracted by looking at the byte definitions from Figure 8. The Figure shows that bytes 17-19 represent the AC output voltage. By first extracting the row that corresponds to the inverter data and then extracting these three bytes, we are able to get a numeric value for the AC output voltage.

The last major component to the diagnostic system is error detection. The primary functionality of this component is to analyze data from the hardware in order to automate error detection and correction to prevent harm to the system and user.

This was achieved by utilizing LabVIEW's case blocks. These cases can perform logical comparisons or cause a new executable file to launch, which will visually communicate with the user that there is a system error. Figure 9 shows an example of an error



**Figure 9: COM Port Error** 

message that occurs when the user has designated the incorrect COM port.

Figure 10 is an example of using a case structure to launch an executable file to visually communicate an error to the user. An executable file gives us the opportunity to customize the error popup to visually communicate what is going on with the system. For users in Sudan, the visual warning is necessary to help them understand what is going wrong. In this case the user is asked if they want to turn off the inverter. If they say yes, a command will be sent to the MATE

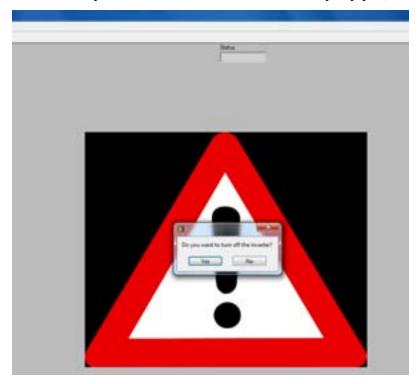


Figure 10: Executable File Popup

and the inverter will be shut down.

Similar messages will be implemented for various errors that could occur in the system. For example, an error message will popup when the battery charge level reaches a critical value. Once the charge drops below 20%, the program will automatically shut down the system to prevent permanent damage to the batteries.

Additional error messages will be integrated into the system in the coming weeks as we start to run the system continuously.

Subsystem Lead Personnel: Enrique Rayon Subsystem Support Personnel: Emmett Perl

#### **Design Specifications**

The design specifications for the power delivery subsystem are shown below in Table 4:

**Table 4: Design Specifications for Mechanical Subsystem** 

Specification	Design
Skid must have the structural capability of supporting all electrical components with a safety factor between 1.5 -2.0	The skid is designed to have a maximum load capacity of 1200 lbs with a safety factor 2.0
Skid must have the capability of being safely transported in the Loma Hall elevator	The skid is designed to weigh no more than 350 lbs to accommodate an elevator load factor of safety of 2.0
Skid must be mobile and have the ability to transport all electrical equipment from one location to another	Skid has four casters two of which will have the ability to swivel and two that will be rigid
Skid must be able to fit through a standard Loma Hall door way	Skid will be designed to have a maximum width/depth of 30 inches and maximum height of 71.25 inches
Skid must be accommodate the ventilation of all electrical equipment to prevent accumulation of thermal energy	The skid will be uncovered on the front, back, left and right side to promote maximum natural convection heat removal.
Skid must be aesthetically pleasing	Skid will have outside frame members welded at 45 degree angles. All sheet metal shelves will be flush with frame.
Skid must facilitate the organization and integration of all electrical equipment	The layout of the skid and volumetric design of each compartment accommodates clean, effective electrical integration.
Skid must allow for easy access to any electrical component	Skid will maintain sufficient space around all components. Minimum of 4 inches around the top and back side.
Skid must contain all fundamental electrical components involved in the USD demonstration	Skid will have three compartments or levels that have sufficient volume to comfortably accommodate all prototype components.

The Skid is designed to be a resource for the USD prototype demonstration for the Critical Design Review, the Final Design Review, and the USD engineering open house event. It is intended to house the major electrical components in a safe, secure, organized, and meaningful manner. In addition to this, the skid must facilitate the presentation and transportation of all electrical components. All of these design specifications can be found in greater detail in Table 4. All the specifications listed in this table have been successfully achieved.

When addressing the skid's ability to house and transport all electrical components, the material selection was a central design variable. To ensure that the skid could handle an overall distributed load of approximately 550 lbs, hollow square tubing was chosen because of its durability, strength, and low cost. Given our established connections with West Coast Iron, Inc. a steel fabrication company in Spring Valley, San Diego, the financial cost of the steel was not an issue. The major tradeoff in using steel as opposed to another building material such as wood is an increase in weight per linear foot. This translates to a heavier skid and thus decreased mobility. This design implication was weighed against the cost, durability, and strength implications in selecting steel as the skid material.

The physical dimensions of the skid were maximized to comfortably accommodate all electrical components. Each compartment was designed to house specific electrical components of the system. Please see Table 13, 14, and 15 in Appendix B.3. for greater detail on this design. The top compartment (Compartment #1) was designed for the AC service panel, the laptop diagnostic unit, and all demonstration loads. This compartment was designed to be 52.25 inches (4.4 ft) high, chest level for an average adult male. The middle compartment (Compartment #2) was designed for the charge controller, inverter, Flexware DC, and Flexare AC. The bottom compartment (Compartment #3) was designed to hold all of the deep cycle batteries. Both the top and bottom compartments have a cross-sectional area defined by a 60 inch length and 18 inch height; these dimensions quantify the compartment openings. The cross-sectional dimensions for the second compartment are a 60 inch length and 25 inch height. The compartment dimensions govern the overall size and weight of the skid in conjunction with the constraints of Loma Hall.

The overall dimensions of the skid as shown in Table 11 in Appendix B.3. allow the skid to meet all Loma Hall physical constraints. Thus the skid is able to fit in the Loma Hall elevator and classrooms. Important design parameters to consider are the height and width of the elevator door opening and the Loma Hall doors. The minimum dimensions here dictate the overall height and width constraints of the skid. The overall width of the skid is 30 inches while the width of the Loma door openings are 35 inches as shown in Table 12 in Appendix B.3. Therefore a 5 inch clearance is achieved. The overall height of the skid is 71.25 inches while the doorway height is 84 inches. Again clearance is achieved. Finally, the maximum weight carrying capacity of the Loma elevator is 2500 lbs. The fully loaded skid weight is 833.3 lbs thus there is a factor of safety of approximately 3 in regards to the elevator load capacity. The other design consideration is due to the skid's fully loaded total weight and the load capabilities of the steel caster plate wheels. Four of these wheels are rated per the Grainger manufacturer specifications for a

maximum weight of 1,800 lbs. Therefore a 2.2 factor of safety is associated with the wheels ability to handle the skid load. This factor of safety is within the design specifications outlined in Table 4.

In addressing the mobility and ventilation design specifications, the skid was designed to maximize natural convection cooling by maximizing the skid open area. For this reason, the back, front, left and right sides of the skid were left uncovered.

The safety and mobility specifications for the skid were achieved by fastening all electrical components to solid 12 gauge sheet metal shelves anchored to steel square tubing. The fastening of all electrical components enables the safe transportation of skid from one location to another. The other important design consideration taken into account is the tendency for the skid to tip. This occurrence was minimized by concentrating 88% of the component load on the lower half of the skid, essentially lowering the skid's center of gravity and thus decreasing its propensity to tip.

The aesthetic design specification was achieved by recessing the steel square tubing frame members and minimizing the visibility of welds. All external conspicuous welds were eliminated with a metal grinder. In addition, the recessing of steel members particularly the edge and inner supports allowed the sheet metal shelving to be flush with the outer skid frame connectors. Lastly the physical strategic arrangement of the electrical components within the skid promotes an organized and easily identifiable perspective of the prototype electrical components.

#### Subsystem Current Status

The current status of the Skid mechanical engineering subsystem is marked by completion of the skid construction and the mounting of all the prototype electrical system components. Please see Appendix B.4.4. for all of the mechanical drawings of the assembled Skid and the mechanical drawings for the subcomponents. The physical specifications for all procured items can be found in Appendix B.4.1. Please also refer to Table 7 for a detailed Bill of Materials for the metal frame subcomponents of the skid assembly found in Appendix A.

The following is a summary of the build process including inspections, evaluations, the build procedure, and the mounting procedure.

#### **Initial Material Evaluation**

The first step in the build process was to validate and inspect all skid components to verify accuracy and precision of the critical physical dimensions. All the square steel tubing was measured and inspected for material defects. The sheet metal and caster wheel plates were also evaluated in a similar but less critical fashion.

#### Machining

After inspecting the material it was discovered that two of the frame columns, four of the inner supports and two of the frame connectors were not cut to the appropriate lengths. These assembly subcomponents and parts were identified and cut to the appropriate lengths. In addition, the four quarter inch wheel plates were machined according to the engineering assembly subcomponent drawing found in Appendix B.4.4. All of these machined parts were then deburred using a metal grinder.

#### **Assembly via Weld Connections**

The construction of the Skid was defined by assembling the steel frame using a series of welded T-Corner (TC) Butt joints. After analyzing the build process it was decided that the most effective approach to assemble the frame was to begin with the four components that comprise one side of the frame, two frame columns, and two frame connectors. These four components were welded together to establish one side of the frame. Subsequent to welding and inspecting the four joints, this procedure was repeated for the opposite side of the skid to establish both sides of the outer skid frame.

After establishing the outer skid frame the locations of the three compartments were marked using a black felt marker. The aforementioned compartment locations refer to the location of each of the 28 hollow square steel compartment supports. These 28 members consist of 17 edge supports, 3 top supports and 8 inner supports. These locations specified by the engineering drawings were carefully checked and inspected multiple times before proceeding to assemble the rest of the skid.

Using the previously marked and measured locations, 2 inner supports were welded at the extreme upper right and upper left corner of one of the two four member outer frames. 2 inner supports were welded at the extreme lower right and lower left corners of one of the four member outer frames. Subsequent to welding and inspecting these four joints, the remaining 3 top supports were welded onto the same four member outer frame. All welds were then inspected before proceeding to weld the remaining 4 inner supports and 17 edge supports to the same outer frame. From the engineering drawings it can be seen that there are 5 edge supports that comprise the middle and bottom compartment. The top compartment is comprised of only two edge supports. Each of the welds was then inspected and re-worked as needed. Subsequent to this build evaluation the complementary four member outer skid frame was then welded at each support location to the other four member outer skid frame. The two inner supports at the extreme upper left and right hand corner were welded first. This was followed by the two inner supports at the extreme lower left and right hand corners of the frame. Next the remaining 3 top supports were welded, followed by the remaining 17 edge supports and 4 inner supports. At this point both four member outer skid frames were connected via butt joint welds by 17 edge

supports, 8 inner supports, and 3 top supports resulting in 56 weld locations. These 56 welds were then inspected, reworked, and aesthetically refined with a grinder as needed.

Lastly the wheel plates were welded to the bottom of the skid frame as indicated in the skid assembly engineering drawing in Appendix B.4. The ¼ inch wheel plates facilitated the attachment of the 4 Grainger caster wheels. Two swivel wheels were welded to the base plates on one side while two rigid wheels were welded to the opposite side. The pairing of swivel and rigid wheels was employed to improve skid control during transportation.

Finally, the four 12 gauge sheet metal shelves were then inserted into the four shelf compartments and lightly spot welded to secure them to the frame. A global evaluation of the skid was conducted by the Vice President of West Coast Iron, Inc. Enrique Rayon Sr. All weld joints were inspected, reworked, and aesthetically refined as needed.

#### **Equipment Mounting**

The next aspect of the skid build process was to locate and drill the appropriate holes for the electrical components. The first step was to situate the electronic components on the skid in order to visualize the physical arrangement of all the components and evaluate the feasibility of the electrical interconnections. This process was carried out by the entire team. The primary considerations taken into account at this step were the electrical integration, electrical safety, aesthetics/appearance, and component fastening to the skid structure. Once agreed upon, locations were confirmed. These locations were marked and recorded. Using these marked locations the components were secured to the skid via number 8 crown bolt zinc plated self drilling screws, mounting plates, and straps. Equipment such as the FlexPower unit came with mounting plates that were used to secure the unit to the skid. Other components such as the batteries were strapped to the skid during transportation. The crown bolt zinc plated self drilling pan head Phillips metal screws were anchored to both the 14 gauge sheet metal as well as the steel tubing to secure the electrical components.

The last mounting procedure was to secure all demonstration items: light fixtures, electrical outlets, and electrical switches. The light fixture was directly mounted to the top compartment of the skid while the electrical outlets and switches were mounted to wooden blocks which were then secured to the skid. The mounting of demonstration items to wooden blocks was achieved using zinc plated crown bolt number 8 wood screws. The location and presentation of all demonstration items is a key design aspect to the design. It is for this reason that this task was accomplished last. Several different component arrangements were explored for visual appeal as well as electrical integration feasibility.

#### **Weld Procedure Specification & Analysis**

This section of the report will discuss the welding employed in the Skid build process. Specifically, it will address the welding codes, the weld type, weld process, and welding strength.

The welding procedure and parameters employed to assemble the Skid are in accordance with the American Welding Society (AWS) Structural Welding Code for Steel approved by the American National Standards Institute (ANSI).

The weld process employed was multi-pass fillet welding using inert gas metal arc welding (GMAW). The inert gas used was 100% CO<sub>2</sub> set at a flow rate of 30-50 CFM (AWS, 2010). The base metal material specification used in the skid is ASTM A-36 and the filler metal AWS specification is A5.20 with an AWS classification of E71T-1 (Excel Arc) (AWS, 2010).

The general welding technique employed was a vertical progression in the upward direction of the welding gun using a stringer technique with the contact from the tube to the work piece characterized by a distance of 0.5-1.0 inches. There was no peening and the inter-pass cleaning was performed with a wire brush. The GMAW equipment used was semi-automatic (AWS, 2010).

The general welding procedure used the class A5.20 filler metal with a wire diameter of 0.045 inches in conjunction with a current setting of 125-255 Amps with 22-24 Volts. The travel speed of the weld gun and the number of passes or layers were variable parameters manipulated as required (AWS, 2010).

Heat treatment was utilized in accordance with the AWS structural welding code for steel. The preheat minimum temperature for the base metal was attained from AWS Table 3.1 D1.1-96. The minimum temperature was found to be 70 degrees Fahrenheit for the base metal. The maximum inter-pass temperature was 500 degrees Fahrenheit (AWS, 2010).

The mechanical properties as well as the chemical analysis for the welding procedure was based on WestAir Gases and Equipment testing information. In terms of the mechanical properties the tensile strength is 87,000 psi, the yield strength is 76,000 psi, and the elongation is 2 inches (Weld Strength Calculations, 2010). The chemical analysis of the weld for the aforementioned welding procedure is 0.043 Carbon, 1.311 Maganese, 0.746 Silicon, 0.050 Chromium, 0.01 Aluminum, 0.019 Phosphorus, 0.01 Sulfur, 0.016 Molybdenum, 0.028 Nickel and 0.02 Vanadium.

#### 2.3. Test Plan

Each of the four subsystems detailed in the section above are integrated smoothly into the prototype system as a whole. The safety subsystem is directly incorporated into the power delivery subsystem in the combiner box, Flexware DC, Flexware AC, and AC service panel.

Circuit breakers housed in these four enclosures are placed between each major electrical component to protect all the wires and equipment in the system. Ground fault circuit interrupters are used in both the AC and DC sections of the system to protect people from electrical hazards.

The diagnostic subsystem is integrated using the OutBack HUB and MATE. The inverter, charge controller, and Flexware DC have outputs which send data to the HUB and MATE via CAT 5 cables. This data is uploaded to a laptop which is powered by the system.

The mechanical subsystem is used to house many of the electrical components which belong to each of the other three subsystems. This includes the inverter, charge controller, batteries, Flexware enclosures, AC service panel, and all of the loads. The entire diagnostic subsystem is housed on the mechanical skid as well as many components from the safety and power delivery subsystems.

Each subsystem will be tested individually. The power delivery subsystem will be tested using a digital multimeter and data from the MATE. The digital multimeter will read the voltage and current at each point in the system to make sure that it is running properly. In addition to reading the DC power levels, we will also test the AC frequency and voltage to make sure that the inverter is functioning properly. Data from the inverter, charge controller, and batteries will also be used to assess the power delivery subsystem. By reading this data in the diagnostic program, we are able to tell what is going on in the system without exposing ourselves to any dangerous electrical hazards.

Each of the circuit breakers in the safety subsystem will be tested. This will be done by shorting each circuit to force them to exceed their current rating. This test will assure that the grounding wire is connected correctly and that each circuit breaker is functioning properly. In addition, the ground fault circuit interrupters can be checked using a test button to ensure that they are working.

The diagnostic subsystem will be tested primarily using a debugging process. When the system is turned on, the diagnostic program will be running continuously and will constantly be storing data to text files on the computer. We will incur various errors that will show up in the program to make sure that it is diagnosing them correctly. By exposing the program to many different errors, we will be able to find when the program malfunctions and debug it so it works correctly.

The design testing for the mechanical subsystem will include accurate and precise physical and thermal measurements. The physical measurements will focus on the weight of the fully loaded skid assembly, which will be compared with the physical constraints shown in Table 4. The thermal analysis will consist of temperature readings of the inverter and batteries using the Remote Temperature Sensor. The final design aspect that will be explored is skid mobility. Various skid attachments such as handles and straps will be examined as possible solutions to improve mobility of the skid.

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## **Appendix A: Complete Parts List**

A complete parts list for the system and the skid are shown below in Tables 5, 6, and 7:

**Table 5: Overall Parts List** 

	Skid Mounting						Mechanical Skid						Safety Subsystem							Diagnostic Subsystem				Energy Storage Subsystem				Power Generation Subsystem									Power Delivery Subsystem				Lighting Subsystem	Linkfing Cubanation								1 Overall Solar Power System	Quantity
8 Douglas Fir Green Lumber 100 Zinc Plated Steel Crown Bolt 100 Zinc Plated Steel Crown Bolt			2 Rigid Wheel Plate Caster	2 Swivel Wheel Plate Caster	1 1.0" Steel Square Tubing	1 14 USS Gauge Sheet Metal		c	1 Flexware Surge Protector	1 Terminal Bus Bar	1 120 Amp AC Breaker	1 80 Amp DC Breaker			1 Laptop	1 LabVIEW	1 RS232 to USB Cable	1 HUB 10	1 MATE			3 2/0 Battery Cables	2 4/0 Rattery Cable			1 6 Gauge Transmission Wires	1 Combiner Box	6 TSM 230 PA05 Solar Panels		1 14 Gauge Wire	1 Conduits	1 Standard Outlet	1 5 Piece Outlet Adapter	1 Brooker Basel	1 FlexMax 60 Charge Controller	1 Remote Temperature Sensor	1		1 Light Switch	2 EML 4-1x4-4L54	4 RWI -2-1-x4-31-32-HP		1007 10011	1 Meck Boom	1 Safety Subsystem	1 Diagnostic Subsystem	1 Energy Storage Subsystem	1 Power Generation Subsystem	1 Power Delivery Subsystem		ntity Item
Home Depot Home Depot			West Coast Iron, Inc.	West Coast Iron, Inc.	West Coast Iron, Inc.	West Coast Iron, Inc.			OutBack Power	OutBack Power	OutBack Power	OutBack Power			Dell	National Instruments	Cables Unlimited	OutBack Power	OutBack Power			Anixter Wire Co.	Anixter Wire Co.	1		Coleman	OutBack Power	Trina		Coleman	Tweco	Stay Online Corp	Wonpro	DI Coo		OutBack Power			Heath Zenith	P-2 Lighting	P_2 I inhting										Manufacturer
Home Depot Home Depot				Grainger	All Metals Inc.				OutBack Power	OutBack Power	OutBack Power	OutBack Power					Fry's Flectronics	Infinigi	Infinigi			Anixter Wire Co.	Anixter Wire Co.	1		USD	OutBack Power	IISD/AM Solar		USD	Home Depot	stayonline.com	110220Volts.com		AM Solar	OutBack Power			Home Depot	P-2 Lighting	P.2 Lighting										Source P
\$19.28 iLevel S4S \$5.58 #8 Phillips Wood Screw http://www.homed \$5.58 #8 Phillips Metal Screw http://www.homed \$30.84 total SM		\$1,290.84 total MS	\$44.06 Load Capacity 450lbs	\$54.30 Load Capacity 450lbs	\$596.07 Hss 1" X 1" X 1/8"	\$267.88 Hot Rolled Sheet Metal		\$387.51 total SS	\$193.73 FW-SP-ACA	\$113.76 ODD-GFF-800-123VDC	\$38.00 OBB-60D-480VAC-DIN	\$23.00 OBB-80-150VDC-PNL		\$800.74 total DS	\$0.00 Michael Rios' Laptop	\$0.00 USD Licence	\$21.99	\$281.38	\$222.22		\$246.93 total ESS	\$48.00 Pending Donation	\$190.00 Pending Donation	7000	\$438.06 total PGS	\$0.00 Existing Wire to L311	\$126.22	\$311.84 Borrowing from AM	4	\$6.383.83 total PDS	\$22.00 From Vent in L311	\$3.00 Type D Outlet	\$9.99 C and D adaptor	\$169 95 220V 50 Hz	\$530 00 Borrowing from AM	\$34.94	\$5 500 OF D	\$799.09 total LS	\$23.00 Donated by P-2 Lighting	\$338.24 Donated by P-2 Lighti	\$437.85 Donated by P.2		\$10,377.84 Total system cost	\$1,290.84 West Coast Iron, Inc.	\$387.51 OutBack Power	\$800.74 LabVIEW	\$246.93 Trojan Batteries	\$438.06 AM Solar	\$6,383.83 OutBack Power		Price Notes
http://www.homedepot.com/fi.eve/h.d/1/N-5yc1/85og/R-2/0094172/h.d2/Podu- www.http://www.homedepot.com/h.d1/N-5yc1v/R-1/0349329/h.d2/ProductDisplay/ www.http://www.homedepot.com/h.d1/N-5yc1v/R-1/0337521/h.d2/ProductDisplay/				er.com	http://www.allmetalsinc.com/steelsquaretube/T100100125.html	http://www.allmet											ntp://www.butbackpower.com/aocinian/1401103033023iiextiet_ac.but	http://www.outbackpower.com/docman/1401103031354hub.pdf										http://nadsonsale.com/PA05.pdf							http://www.outhacknower.com/docman/1401102020748fleymay.ndf	http://www.outpackbower.com/docinal// 1061030303 tollexbower.wo.bul			ing	\$338.24 Donated by P-2 Lighting http://www.p-2.com/cutsheet/outdoor/EWB.pdf	http://www.p-2.com/cutsheet/general_indoor/RWI_ndf										Link

## **Table 6: Skid Parts List**

Material	Supplier/Vendor	Material Description	Product Code	Dimensions	Weight (lbs/ft <sup>2</sup> )	Length (ft)	Quantity	Cost	Materia
Sheet Metal	All Metals Inc.	14 USS Gauge Steel (Hot Rolled)	N/A	W 60" x L 120"	3.125	N/A	1	\$ 267.88	\$
									\$
Vheel Plate Caster	Grainger	Load Capacity 450lbs, Swivel, Overall height 6-3/8"	4W900	D 5" X W 1-1/2"	1	N/A	2	\$ 27.15	\$
Vheel Plate Caster	Grainger	Load Capacity 450lbs, Rigid, Overall height 6-3/8"	4W903	D 5" X W 1-1/2"	2	N/A	2	\$ 22.03	\$
									\$
teel Square Tubing	All Metals Inc.	Hss 1" X 1" X 1/8" (Grade A500)	N/A	1" X 1" X 1/8"	1.436	80.33	N/A	\$ 7.42	\$
teel Square Tubing	All Metals Inc.	Hss 3/4" X 3/4" X 1/8" (Grade A500)	N/A	3/4" X 3/4" X 1/8"	0.753	46.67	N/A	\$ 7.04	\$

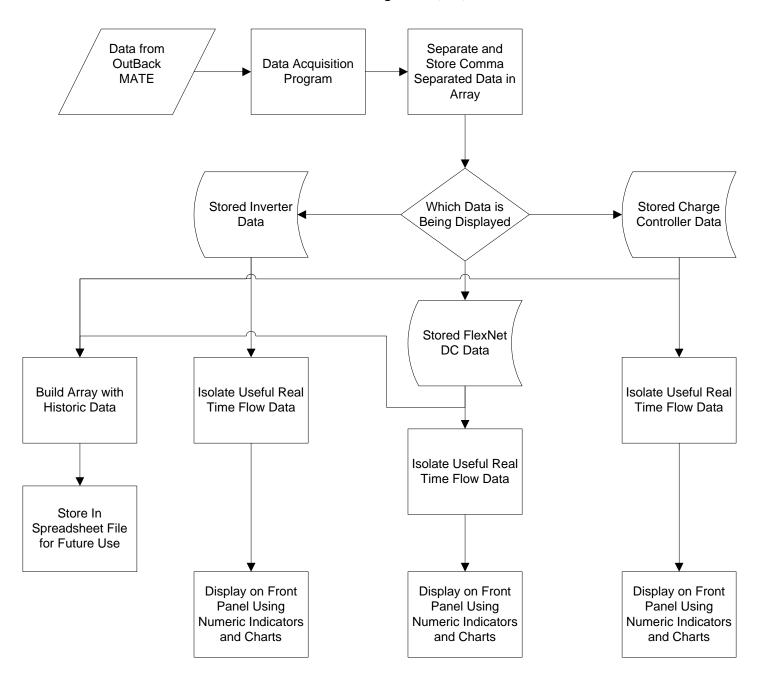
**Table 7: Skid Bill of Materials and Specifications** 

Material	Height (in)	Width (in)	Length (in)	Area (in²)	Weight (lbs)	Volume (in <sup>3</sup> )	Quantity
Top Sheet	0.1046	28	60	1680	36.5	175.728	1
Interior Sheet	0.1046	30	60	1800	39.1	188.28	3
Sheet Metal Total				7080	153.6	740.568	4
Material	Height (in)	Width (in)	Span/Length (in)	Area (in <sup>2</sup> )	Weight (lbs)	Volume (in <sup>3</sup> )	Quantity
Frame Columns	1	1	65	65	7.78	65	4
Frame Connectors	1	1	60	60	7.18	60	4
Inner Bracing Supports	1	1	28	28	3.35	28	8
Outer Supports	1	1	60	60	7.18	60	4
Edge Supports	0.75	0.75	28	21	1.76	15.75	17
Top Supports	0.75	0.75	28	21	1.76	15.75	3
Square Tubing Subtotal 1	0.75	0.75	560	420	115.36	964	20
Square Tubing Subtotal 2	1	1	964	964	35.14	315	20
Steel Square Tubing Total			1524	1384	150.5	1279	40
Material	Height (in)	Width (in)	Span/Length (in)	Area (in <sup>2</sup> )	Weight (lbs)	Volume (in <sup>3</sup> )	Quantity
Grainger Swivel Wheels	6.375	N/A	N/A	N/A	2.35	N/A	2
Grainger Rigid Wheels	6.375	N/A	N/A	N/A	2.13	N/A	2
Wheel Base Plates	0.25	4	4	16	1.50	4	4
Steel Square Tubing Total			4	16	6.0	4	8
		_					
TOTAL				8480.0	310.1	2023.6	52

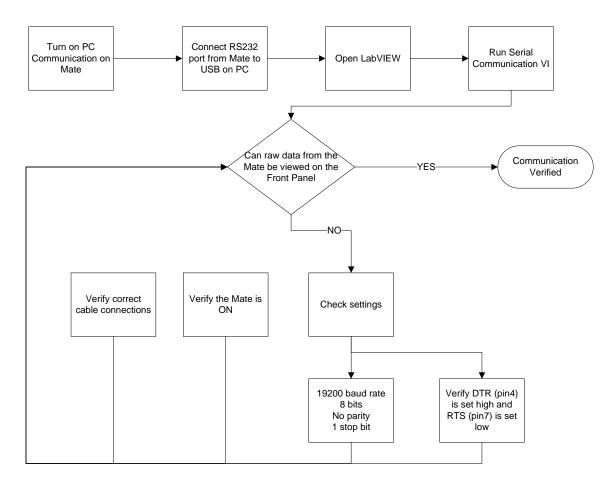
### **Appendix B: Technical Design Documents**

#### Appendix B.1. Flow Charts and Code

All the flowcharts and code are shown below in Figures 11, 12, and 13:



**Figure 11: Power Flow Program Flow Chart** 



**Figure 12: Serial Communications Flowchart** 

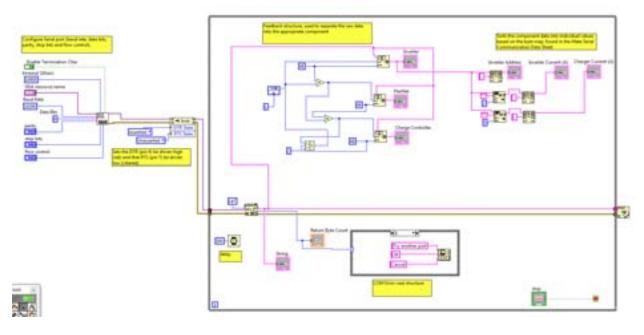


Figure 13: Diagnostics LabVIEW Code

#### **Appendix B.2. Electrical Safety Design**

This section details the electrical safety design for the entire system. This includes the wire ampacity calculations and wire sizing tables.

#### Wire Sizing

When sizing the wires, the most important criteria to consider is the ampacity and the voltage drop. Ampacity refers to the current carrying capacity of the wire; the larger the wire, the more it can carry. The system must be wired with proper wire sizes to minimize losses and to prevent the wires from overheating.

To calculate the required amperage (According to NEC Requirements) of the wire that connects the array to the batteries, the rated short circuit current of the module is multiplied by a factor of 1.25 twice to ensure that the wire can handle any current surges produced by the panels caused by reflection or exceptionally sunny days. The calculations are shown in Table 8 below. The required amperage of the wire connecting the storage system to the loads is the inverter rated watts divided by the inverter efficiency and divided by the DC system voltage. This gives the maximum load current which is then multiplied by 1.25 to provide for a factor of safety. This ensures that the conductor never carries more than 80% of its rated capacity. Calculations for this section are below in Table 8.

System Wire Sizing: All According to NEC Requirements PV to Inverter Module Short Circuit Current (Rated) # modules in parallel NEC Factor of Safety 1 NEC Factor of Safety 2 Required Amps Total Amps 2.00 16.62 25.97 8.31 1.25 1.25 Inverter To Loads DC system voltage NEC Factor of Safety 2 Required Amps Inverter Watts (Rated) Inverter Efficiency Total Amps 0.90 48.00 83.33 1.25 3600.00 104.17 PV to Combiner Box Module Short Circuit Current (Rated) NEC Factor of Safety 1 NEC Factor of Safety 2 Required Amps 1.25 1.25 12.98 8.31

**Table 8: Wire ampacity ratings** 

#### Voltage Drop

The second consideration for wire sizing is the voltage drop, which is a measurement of the decrease in voltage due to a wire's resistance and length. This can be analyzed by equating the wire size to the amp rating. These relationships can be seen below in Table 9. Since our system will be implemented over a relatively short range, voltage drop will not be a factor of concern for power loss. This is because the largest wires in the system will run a very short distance (less

than 50 feet). For example, the maximum wire length we can use for the wire that runs from the array to the storage system is 74.3 feet, but in reality we only need about 20 feet. The same thing goes for the wire connecting the storage system to the AC load center. The max length that we can use there is 64 feet, but only about 10 feet of that is needed for this system.

Table 9: 5% voltage drop and wire length table

	48-V	OLT SYS		
Total		Wi	re size	
watts	12	10	8	6
		length of	wire run (fe	et)
6	4,683	7,442	11,867	18,824
7	4,014	6,379	10,171	16,134
8	3,512	5,581	8,900	14,118
10	2,810	4,465	7,120	11,294
12	2,341	3,721	5,933	9,412
13	2,161	3,435	5,477	8,688
14	2,007	3,189	5,086	8,067
16	1,756	2,791	4,450	7,059
18	1,561	2,481	3,956	6,275
20	1,405	2,233	3,560	5,647
21	1,338	2,126	3,390	5,378

#### Wire Gauge Selection

Wire Gauge selection is based on several factors; the wire carrying capacity (ampacity), temperature, location covering, insulation, and outer jacket type. Theou Village is located in a region that is very hot and dry for approximately half the year and wet for the other half so these factors are very important in selecting the type of wiring that will be used in this system. Based on the wire sizing calculations from Tables 8 and 9 above, the wire connecting the array to the storage system must be able to carry at least 25.97 Amps and the one from the storage system to the loads must be able to carry a total load of 104.17 Amps. Type THWN will be selected because it best fits all the weather related criteria of the region. Since THWN is not available for 60°C (140°F), selection will be made under 75°C (167°F). Taking all these factors into account, the gauge selections (NEC) are AWG #10 (American Wire Gauge #10) from the array to the storage system and AWG #2 from the storage system to the loads. All wires are copper.

**Table 10: NEC Table 310.16 showing wire gauge ratings** 

	Temperature Rating of Conductor		
	60°C (140°F)	75°C (167°F)	90°C (194°F)
Size AWG or kcmil	Types TW, UF	Types RHW, THHW, THW, THWN, XHHW, USE, ZW	Types TBS, SA, SIS, FEP, FEPB, MI, RHH, RHW-2, THHN, THHW, THW-2, THWN-2, USE-2, XHH, XHHW, XHHW-2, ZW-2
		(	COPPER
18	-	-	14
16	-	-	18
14*	20	20	25
12*	25	25	30
10*	30	35	40
8	40	50	55
6	55	65	75
4	70	85	95
3	5	100	110
2	95	115	130
1	110	130	150
1/0	125	150	170
2/0	145	175	195
3/0	165	200	225
4/0	195	230	260

#### Disconnects

Each piece of equipment in a PV system, such as charge controllers, inverters, and batteries must be able to be disconnected from all sources of power (NEC 690.15). The requirements of what a disconnect must be include:

- They can be switches or circuit breakers
- They must not have any exposed live parts
- They must plainly indicate whether they are in the open or closed position
- They must be rated for the nominal system voltage and available current (NEC 690.17)

#### Overcurrent Protection

The NEC requires that every ungrounded conductor be protected by an overcurrent device (NEC 240.20). This provides multiple levels of protection for the vital electrical components of the Inverter/Charger in the event of an electrical surge or nearby lightning strike. The selected FW-

SP-250 will protect the two inverter/chargers via thermally fused Metal Oxide Varistors (MOVs). Furthermore, since this is designed to operate between 120 to 240 VAC at 50/60 Hz and 12 to 48 VDC, it meets this systems' voltage and frequency requirements of 230 VAC and 50 Hertz.

#### Appendix B.3. Mechanical Subsystem BOMs and Physical Specifications

This section includes tables for the skid dimensions, physical constraints, and specifications. Table 11 shows the overall physical specifications of the skid assembly.

**Table 11: Skid Assembly Overall Physical Specifications** 

Overall Skid Dimensions								
Height (in)	Width (in)	Length/Depth (in)	Area (in²)	Volume (in <sup>3</sup> )	Weight (lbs)			
71.25	60	30	4402.5	132075	833.3			

Table 12 illustrates the physical constraints of moving the skid through Loma Hall.

**Table 12: Loma Hall Physical Constraints** 

Loma Doors and Elevator Constraints								
	Height (in)	Width (in)	Length/Depth (in)	Area (in²)	Volume (in <sup>3</sup> )			
Elevator	90	82	52.5	7380	387450			
Elevator Door Way	84	42	N/A	3528	N/A			
Door Way	84	35	N/A	2940	N/A			

Table 13 shows the electrical component specifications for the equipment that will be mounted on the skid.

**Table 13: Electrical Component Specifications** 

Electrical Component Physical Dimensions									
Component	Weight (lbs)	Height (in)	Length (in)	Width (in)	Area (in <sup>2</sup> )	Volume (in <sup>3</sup> )			
Laptop	17	12	16.5	12	198	2376			
Charge Controller	12.2	16.25	5.75	4	93.44	373.75			
AGM Concorde									
Battery	182	12.94	7.06	10.28	182.71	1878.29			
Flex Power Unit	232	20.25	46.5	13	941.63	12241.13			
Breaker Box Unit	30	9	14.1	4.1	126.90	520.29			
Loads	50	15	5	10	75	750			
Total	523.2				1617.7	18139.5			

Table 14 shows the specifications for each compartment in the skid

**Table 14: Compartment Specifications** 

Skid Compartment Physical Dimensions									
Height (in) Length (in) Width (in) Area (in²) Volume (in³) W						Weight (lbs)			
Compartment #1	18	60	28	1080	30240	67			
Compartment #2	25	60	28	1500	42000	244.2			
Compartment #3	18	60	28	1080	30240	212			

Table 15 shows how the electrical components relate to the compartment specifications

**Table 15: Electrical Components per Compartment Specifications** 

	Maximum Physical Dimensions of Electrical Components								
	Electrical Components	Max Height (in)	Max Length(in)	Max Width (in)	Total Area (in²)	Total Volume (in <sup>3</sup> )	Total Weight (lbs)		
C1	Laptop and Loads	15	28.22	15	423.3	6349.5	67.0		
C2	Flex Power Unit and Charge Controller AGM Batteries (2) and	16.25	52.25	15	849.1	12736.0	244.2		
C3	Breaker Unit	18	28.22	15	508.0	7619.4	212.0		

## **Appendix B.4. Mechanical Drawings**

This section includes many drawings of the final mechanical skid design. These drawings can be seen below in Figures 14 thru 27.

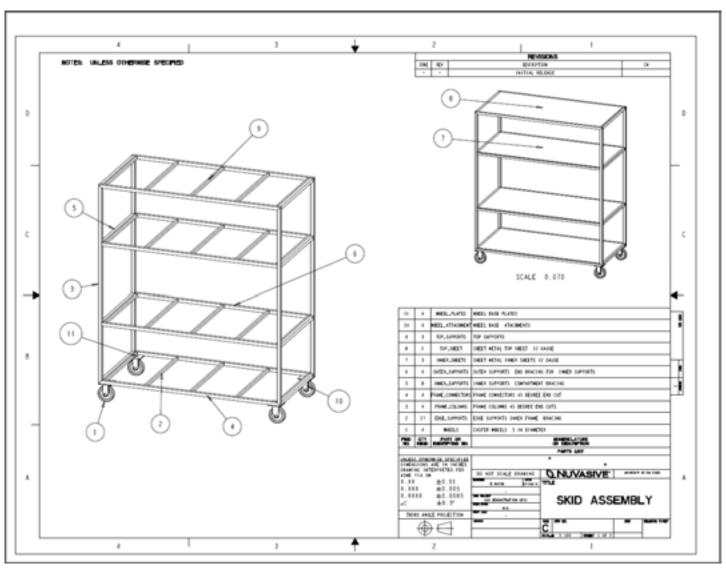


Figure 14: Skid Assembly Drawing 1

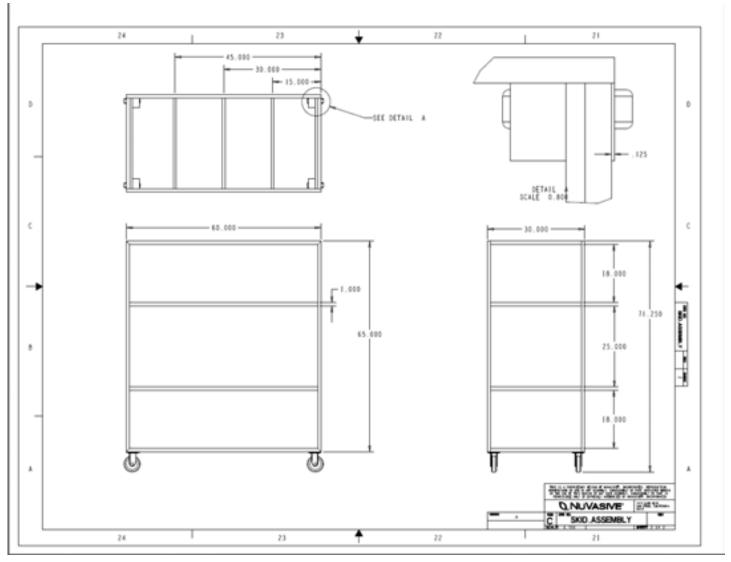
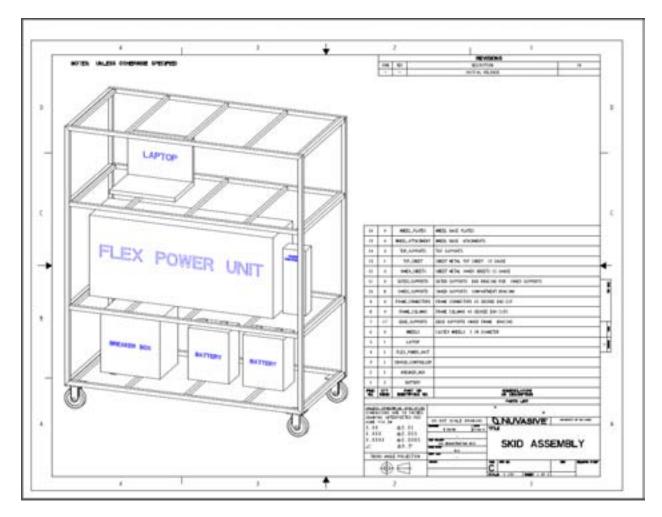


Figure 15: Skid Assembly Drawing 2



**Figure 16: Skid Assembly Drawing 3** 

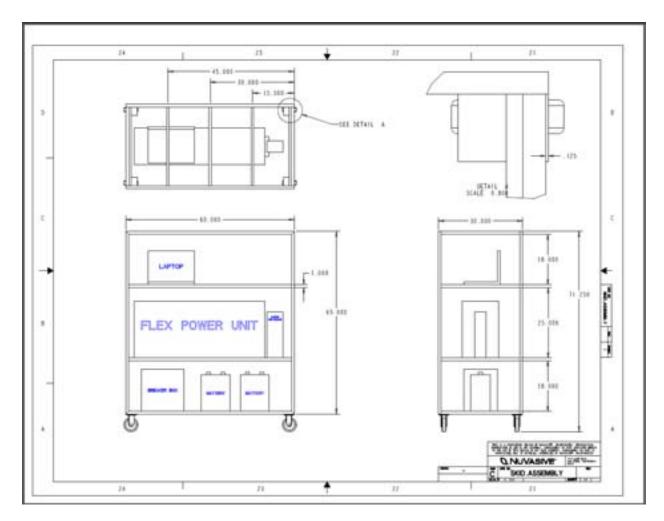
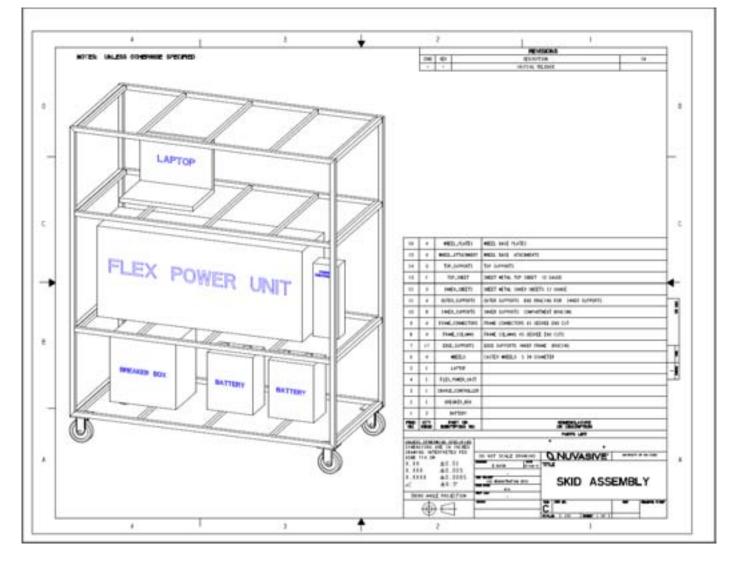
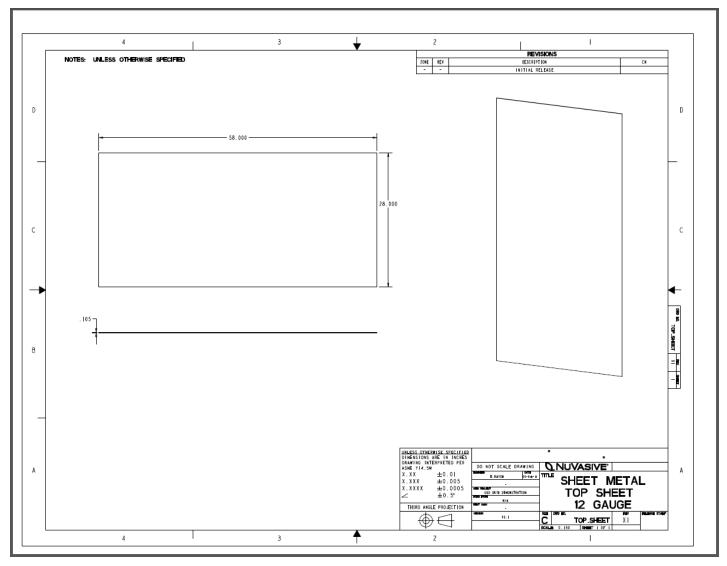


Figure 17: Skid Assembly Drawing 4



**Figure 18: Skid Assembly Drawing 5** 



**Figure 19: Skid Assembly Drawing 6** 

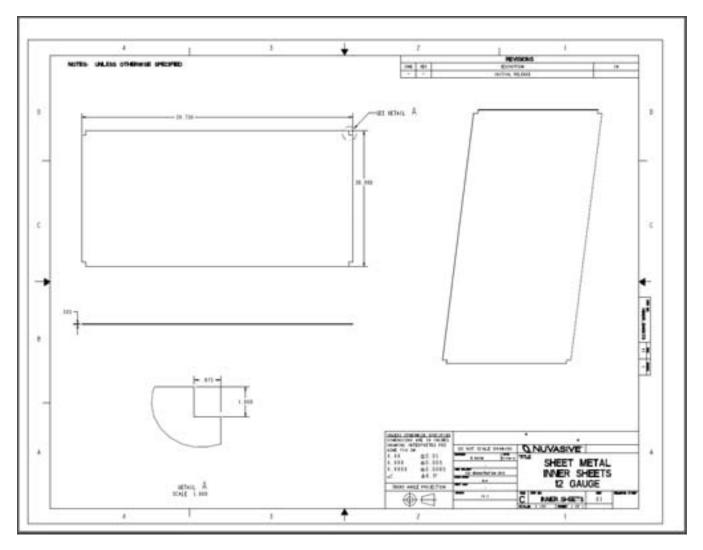


Figure 20: Skid Assembly Drawing 7

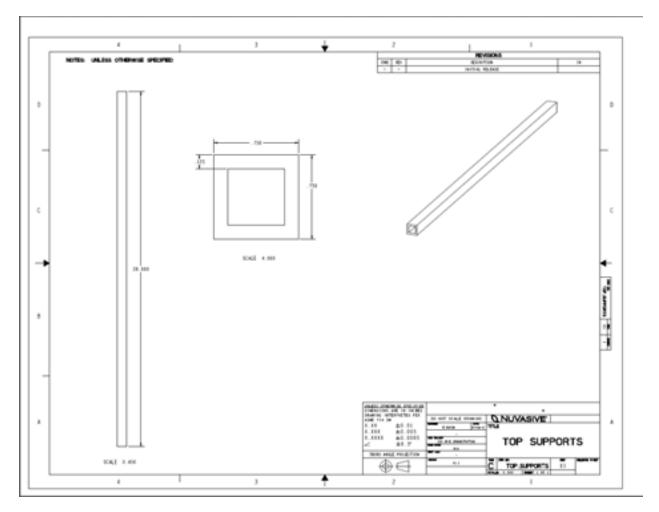


Figure 21: Skid Assembly Drawing 8

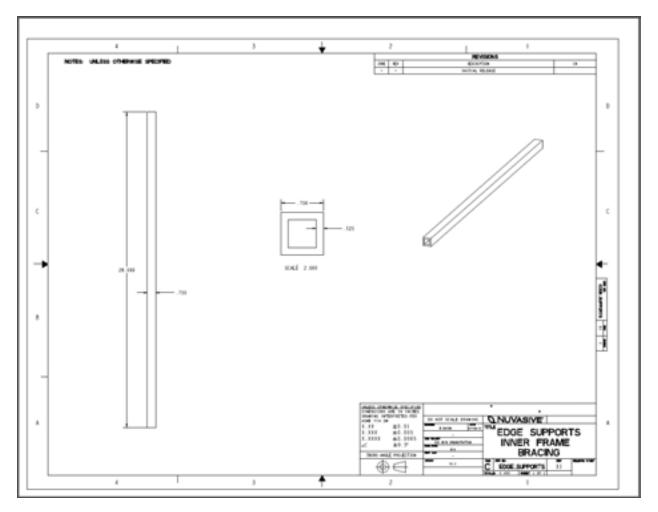


Figure 22: Skid Assembly Drawing 9

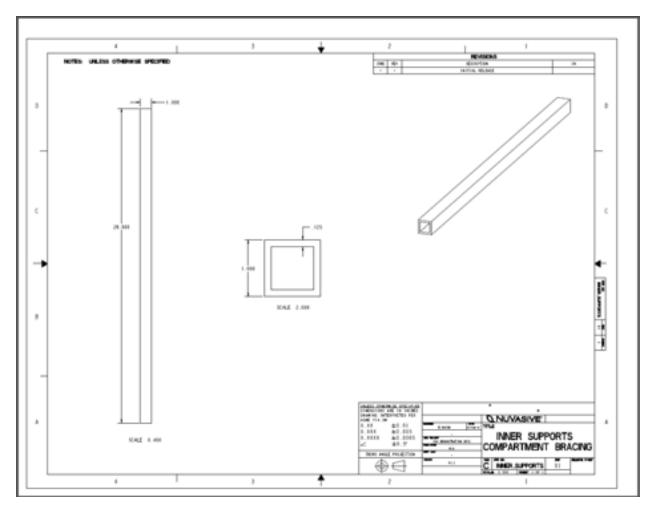


Figure 23: Skid Assembly Drawing 10

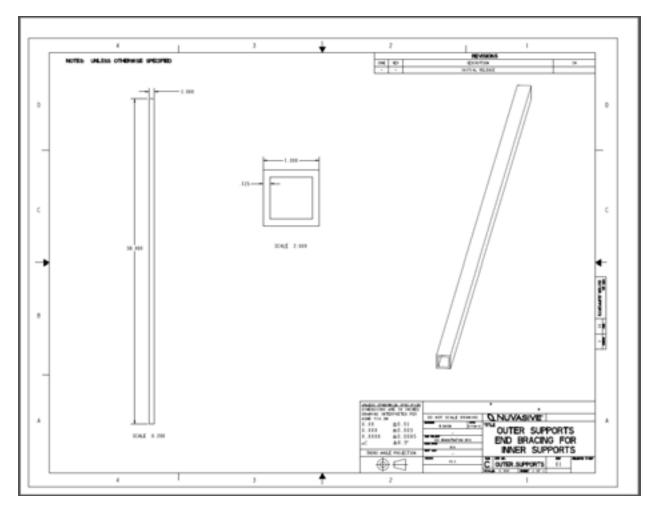


Figure 24: Skid Assembly Drawing 11

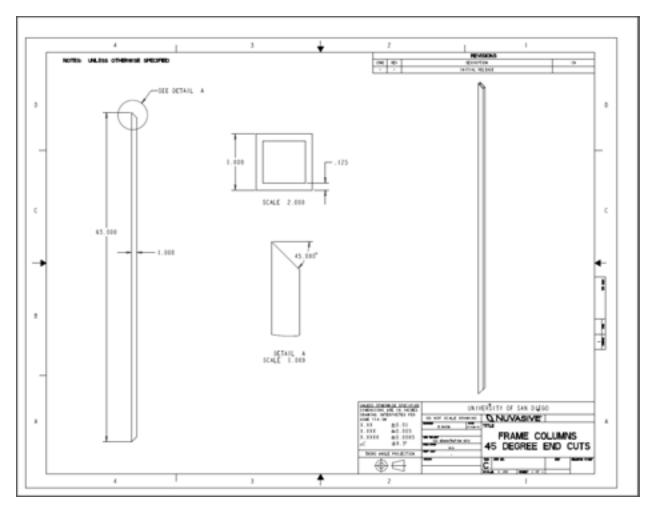


Figure 25: Skid Assembly Drawing 12

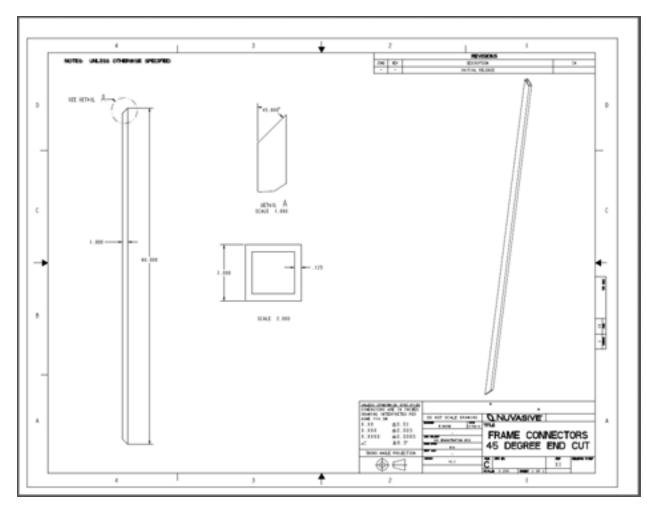


Figure 26: Skid Assembly Drawing 13

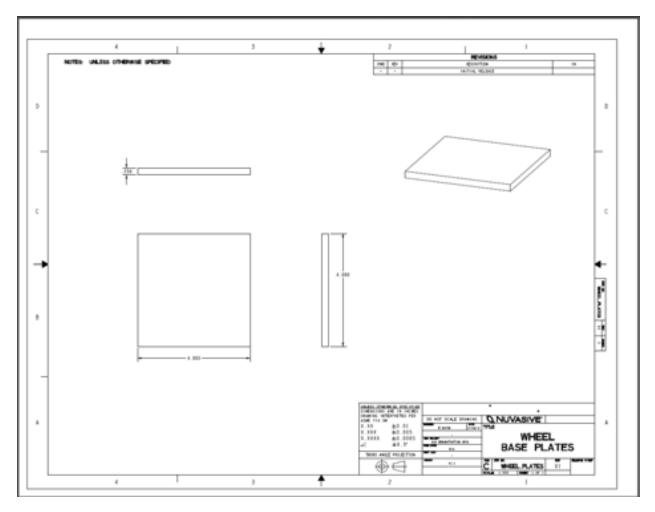


Figure 27: Skid Assembly Drawing 14

## **Appendix B.5. Datasheets**

The datasheets for all of the major electrical components are shown in this section. The datasheet for the VFX3048E OutBack inverter is shown in Figure 28 Below.

		Sealed Models		Vented Models			
		FX2012ET	FX2024ET	FX2348ET	VFX2612E	VFX3024E	VFX3048E
Nominal DC Input Voltage		12VDC	24 VDC	48 VDC	12 VDC	24 VDC	48 VDC
Continuous Power Rating at 25° C (77° F)		2000 VA	2000 VA	2300 VA	2600 VA	3000 VA	3000 VA
ACVoltage/Frequency		230 VAC 50 Hz	230 VAC SO Hz	230 VAC 50 Hz	230 VAC 50 Hz	230 VAC 50 Hz	230 VAC SO Hz
Continuous AC RMS Output at 25°C (77°F)		8.7 amps AC	8.7 amps AC	10.0 amps AC	11.3 amps AC	13.0 amps AC	13.0 amps AC
ldie Power	full	~ 20 Watts	~ 20 Watts	~23 Watts	⇒ 20 Watts	~ 20 Wwm	~ 23 Watts
	Search	~ 6 Watts	~ 6 Watts	+6 Watts	- 6 Watts	- 6 Watts	~ 6 Watts
Typical Efficiency		90%	92%	92%	90%	92%	93%
Total Harmonic Distortion	Typical	2%	2%	2%	2%	2%	2%
	Maximum	5%	5%	jn .	5%	5%	5%
Output Voltage Regulation		12%	22%	12%	±2%	12%	±2%
Maximum Output Current	Feak	26 amps AC	35 amps AC	35 amps AC	28 amps AC	35 arrops AC	35 amps AC
	RMS	20 amps AC	25 amps AC	25 amps AC	20 amps AC	25 amps AC	25 amps AC
AC Overload Capability	Surge	4600 VA	5750 VA	5750 VA	4600 VA	5750 VA	5750 VA
	5 Second	4000 VA	4800 VA	4800 VA	4000 VA	4800 VA	4800 VA
	30 Minutes	2500 VA	3100 VA	3100 VA	3100 WA	3300 VA	3300 VA
AC Input Current Maximum		30 amps AC	30 amps AC	30 amps AC	30 amps AC	30 amps AC	30 amps AC
AC Input Voltage Range (MATE Adjusts	ble) 160 to 300 VAC	160 to 300 VAC	160 to 300 VAC	160 to 300 VAC	160 to 300 VAC	160 to 300 VAC	160 to 300 VAC
AC Input Frequency Range		44 to 56 Hz	44 to 56 Hz	44 to 56 Hz	44 to 56 Hz	44 to 56 Hz	44 to 56 Hz
DC Input Voltage Range		10.5 to 17.0 VDC	21.0 to 34.0 VDC	42.0 to 68.0 VDC	10.5 to 17.0 VDC	21.0 to 34.0 VDC	42.0 to 68.0 VD
Operating Temperature Range		-40° C to 60° C (power denated above 25° C)		-40° C to 60° C (power derated above 25° C)			
Continuous Battery Charge Outp	nd.	100 amps DC	55 amps DC	35 amps DC	120 amps DC	85 amps DC	45 amps DC
Warranty		Standard 2 year / Optional 5 year		Standa	rd 2 year / Optional 5	year	
Weight Unit		62.2 Be (28.4 kg)		61 lbs (27.7 kg)			
	Shipping	67 lbs (30 kg)		64 lbs (29 kg)			
Dimensions (H x W x L)	Unit	13 x 8.25 x 16.25"(33 x 21 x 41 cm)		12 x 8.25 x 16.25*(30 x 21 x 41 cm)			
	Shipping	21.75 x 13 x 22°(55 x 33 x 56 cm)			21.75 x 13 x 22" (55 x 33 x 56 cm)		

Figure 28: OutBack Inverter Datasheet

The datasheet for the OutBack FLEXmax 60 Charge Controller is shown in Figure 29 below.

		ØFLEXmax 80 - FM80-150VDC	©FLEXmax-6O - FM60-150VDC
Nominal Sattery V	foliages	12, 14, 36, 48, or 66 VDC (Single model - selectable via	12, 34, 36, 48, or 60 VDC (Single model - selectable via
		field programming at start-up/	field programming at start-upi
Maximum Output Current 80 amp		80 amps at 104° F (40°C) with adjustable current limit	60 amps a 104° F (A0°C) with adjustable current limit.
Maximum Solar A	irray STC Nameplate	12 VDC systems 1250 Watts / 24 VDC systems 2500 Watts /	12 VDC systems 900 Warts / 24 VDC systems 1800 Warts /
		48 VDC systems 5000 Watts / 60 VDC Systems 7500 Watts	48 VDC systems 3600 Watts / 60 VDC Systems 4500 Watts
NEC Recommended So	olar Amy STC Nameplate	12 VDC systems 1000 Watts / 24 VDC systems 2000 Watts /	12 VDC systems 750 Warts / 24 VDC systems 1500 Warts /
		48 VDC systems 4000 Watts / 60 VDC Systems 5000 Watts	48 VDC systems 3000 Watts / 65 VDC Systems 3750 Watts
PV Open Circuit Vo	oltage (VOC)	150 VDC absolute maximum coldest conditions / 145 VDC	150 VDC absolute maximum coldest conditions / 145 VDC
		start-up and operating maximum.	start-up and operating maximum
Standby Power Co	orsumption	Less than 1 Watt typical	Less than 1 Watt topical
Power Conversion	Efficiency	97.5% is 80 Amps in a 48 VDC System - Typical	96.1% @ 66 Amps in at 46 VDC System voltage - Typical
Charging Regulati	ion	Five Stages: Bulk, Absorption, Pisat, Silent and Equalization	Five Stages: Bulk, Absorption, Float, Silent and Equalization
Voltage Regulation	in Set points	10 to 60 VDC user adjustable with password protection	10 to 60 VDC user adjustable with password protection
Equalization Charg	20/4294/2412	Programmable Voltage Setpoint and Duration - Automatic	Programmable Voltage Setpoint and Duration - Automatic
		Termination when completed	Termination when completed
luttery Temperatu	ure Compensation	Automatic with optional RTS installed / 5.0 mW per 1C per	Automatic with optional RTS installed / 5.0 mV per *C per
		2/bateryork	2V hattery cell
Voltage Step-Dow	ve Capability	Can charge a lower voltage battery from a higher voltage	Can charge a lower voltage battery from a higher voltage
		PV array - Max 150 VDC input	PV array - Max 150 VDC input
Programmable Acar	olary Control Output	12YDC output signal which can be programmed for different	12 VDC output signal which can be programmed for different
		control applications (Maximum of 0.2 amps DC)	control applications (Maximum of 0.2 amps DC)
Status Display		3.1" S and backlit LCD screen - 4 lines with 80 alphanumeric	3.1° IS cmi backlit LCD soven -4 lines with 80 alphanumeric
		characteristic	characters total
Remote Display an	nd Controller	Centional Mate or Mate2 with 95232 Serial Communications Fort	Continual Mate or Mate2 with RS232 Serial Communications Port
Network Cabeling		Proprietary network system using RJ 45 Modular Connectors	Proprietary network system using RI 45 Modular Connectors
A STREET		with CAT Se Cable It word	with CAT Se Cubie III wined
Data Logging		Last 126 days of Operation - Amp Hours, Watt Hours, Time in	Last 128 days of Operation - Amp Hours, Watt Hours, Time in
		Float, Peak Watts, Amps, Solar Amay Voltage,	Floot, Peak Watts, Amps, Solar Array Voltage,
		Max Battery Voltage Min Battery Voltage and Absorb for each	Max Suttery Voltage Min Suttery Voltage and Absorb for each
		day along with total Accumulated Amp Hours,	day along with total Accumulated Amp Hours,
		and I/W Hours of production	and kW Hours of production
Hydro Turbine Apo	olications	Consult factory for approved Turbines	Consult factory for approved furbines
Positive Ground A		Requires two Role Breakers for switching both positive and	Requires two Pole Breaken for patiching both positive and
	***************************************	Negative Conductors on both Solar Array	Negative Canductors on both Solar Array
		and Battery Connections (HJB 4 and HJB 10 can not be used	and Battery Connections (HLB 4 and HLB 10 can not be used
		for use in positive ground applications!	for use in positive ground applications!
Operating Temper	rofices Dance	Minimum 40" to maximum 60" C Power capacity of the	Minimum -40" to maximum 60" C Power capacity of the
obered stube	same range	controller is automatically denoted when operated above 40° O	controller is automatically desired when operated above 40° ()
Environmental Rat	ene	Indoor Type 1	Indoor Type I
Conduit Frockout	100	One 1"BSownium the back, One1" (35mm) on the left side,	One 1"(35mm) on the back, One1"(35mm) on the left side;
Consult Neckous	9	Two 1"(15mm) on the bottom	Two 1" (35mm) on the bottom
Warranty		Standard 5 year / Assilable 10 Year	Standard 6 year / Available 10 Year
Weight	- Unit	12.20 lbs (5.56 kg)	11.65 to 53 kg
moyn.	- Shipping	12.20 feb (3.36 kg) 15.75 feb (7.30 kg)	14.55 Bo 6.4 kg)
Dimensions	- Singping - Unit	16.25" x 5.75" x 4" (41.3 x 14 x 10 cm) - (H x W x D)	135x575x4*(40x14x10cm)
Dimensions	10.700	16.25 x 5.75 x 4 41.3 x 14 x 10 cm - (F1 x W x 1) 21°x 10.5°x 8.75°(33 x 27 x 25 cm)	13.5 % 5.7 \$ 4 \$40 x 14 x 10 cm0 18 x 11 x 8" [46 x 10 x 20 cm]
ACCOUNT.	-Shipping	Remote Temperature Sensor SETS; HUB 4 HUB 10, MATE MATE 2	Broade Temperature Sensor (BTS) HUE-4 HUE to MATE MATE 2
Options			
Menu Languages		English & Spanish	English & Spanish
Certifications		ETL Listed to UL 1741, CSA C222No. 107.1	ETI, Grand to UL 1741, CSA C22.2 No. 107.1

Figure 29: OutBack Charge Controller Datasheet

The datasheet for the OutBack FWPV-12 Combiner Box is shown in Figure 30 below.

		FWPV-8	FWPV-12
Enclosure Materia	ı	Powder coated aluminum with stainless steel hardware	Powder coated aluminum with stainless steel hardware
Mounting Options		Vertical wall mount, pole mount or sloped roof mount to 14 degrees incline (3 in 12 roof pitch)	Vertical wall mount, pole mount or sloped roof mount to 14 degrees incline (3 in 12 roof pitch)
Enclosure Rating		Outdoor Rainproof, UL Type 3R	Outdoor Rainproof, UL Type 3R
Enclosure Security	•	Padlock hole in chassis and cover for up to 3/8 inch pad lock	Padlock hole in chassis and cover for up to 3/8 inch pad lock
Output Terminals		#14 - 2/0 AWG (2.08 - 67.43 mm²) Two box lug terminals included	#14 - 2/0 AWG (2.08 - 67.43 mm²) Four box lug terminals included
Number of separa	te circuits	One Circuit	One or Two Circuits
Number of 150VD	C breakers	up to 8	up to 12 (two groups of six)
Number of 600VD	C fuse holders	up to 6	up to 8 (two groups of four)
Input Terminal		150VDC Breakers / #14 - 6 AWG (2.08 - 13.3 mm²) 600VDC Fuse / #14 - 10 AWG (2.08 - 5.26 mm²)	150VDC Breakers / #14 - 6 AWG (2.08 - 13.3 mm²) 600VDC Fuse / #14 - 10 AWG (2.08 - 5.26 mm²)
Dimensions	Unit (H x W x D) Shipping (H x W x L)	15.2 x 9.2 x 3.9" (38.7 x 23.3 x 9.9 cm) 4.3 x 9.5 x 19" (10.9 x 24.1 x 48.3 cm)	15.2 x 12.7 x 3.9" (38.7 x 32.2 x 9.9 cm) 4.3 x 13 x 19" (10.9 x 33 x 48.3 cm)
Weight	Unit Shipping	4.4 lbs (2.0 kg) 5.5 lbs (2.5 kg)	5.9 lbs (2.7 kg) 7.4 lbs (3.3 kg)
Certifications		ETL Listed to UL1741, UL67, CSA22.2 #29	ETL Listed to UL1741, UL67, CSA22.2 #29

<sup>\*</sup>Specifications subject to change without notice

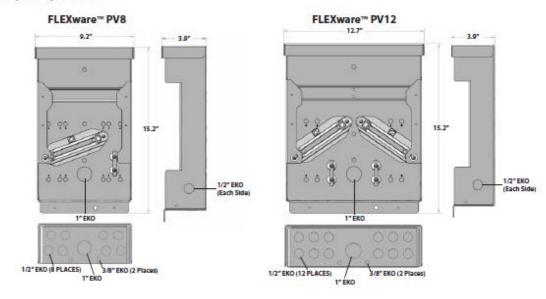


Figure 30: Combiner Box Datasheet

The datasheet for the two FlexWare 500 enclosures is shown in Figure 31 below:

#### Model: FW500-DC

DC enclosure which mounts at the DC side of one or two FX Series Inverter/Chargers. Supports up to six terminal bus bars (not including GBB) and up to three shunt assemblies depending on configuration

**Includes:** Ground bus bar, 500 Amp DC shunt assembly, positive bus, breaker mounting hardware, FW-BBUS and enclosure mounting hardware

UNIT DIMENSIONS (H X W X D)	SHIPPING DIMENSIONS (H X W X L)	SHIPPING WEIGHT	ENCLOSURE TYPE
$18.2 \times 11.4 \times 12.1$ " ( $46.2 \times 29 \times 30.7$ cm)	$14.5 \times 13.4 \times 20.3$ " (36.8 $\times$ 34.1 $\times$ 51.6 cm)	15 lbs. (6.8 kg)	Type-1 indoor (IP30)

#### Model: FW500-AC

AC enclosure which mounts at the AC side of one or two FX Series Inverter/Chargers. Supports six terminal bus bars and one FW-X240. The FW500 system utilizes one FW-MP (mounting plate) and a set of the DCA and ACA conduit adapters for each inverter/charger. DC and AC breakers, Input-Output-Bypass Assemblies and all other additional components sold separately.

Includes: Ground bus bar, DIN mounting bracket, communication cable conduit and enclosure mounting hardware

UNIT DIMENSIONS (H X W X D)	SHIPPING DIMENSIONS (H X W X L)	SHIPPING WEIGHT	ENCLOSURE TYPE
18.2 × 11.4 × 12.1" (46.2 × 29 × 30.7 cm)	14.5 × 13.4 × 20.3" (36.8 × 34.1 × 51.6 cm)	15 lbs. (6.8 kg)	Type-1 indoor(IP30)

Figure 31: FlexWare 500 Datasheet

The datasheets for the OutBack HUB and MATE are shown in Figures 32 and 33 on the next page.

MATE SPECIFICATIONS		
MATE	Grey	Surface mount with RS232
MATE_B	Black	Surface mount with RS232
MATE2	Black	Flush mount without RS232
Interface Display		3.1" (8 cm) backlit LCD - four line, 80 alpha numeric characters
Control Keypad		6 backlit silicone keys - dedicated inverter and AC input keys
Status Indicators		Two LED Status Indicators - AC input (yellow), inverting (green)
Communication Protocol		Proprietary OutBack Multi-drop using an OutBack HUB4 or HUB10
Interconnection Cabling		Standard CAT 5 network cable with RJ45 modular jack - 10' (3 m) included
PC Computer Interface		RS232 opto-isolated DB9 jack 9600 baud serial communication
Microprocessor		16 MHz low power consumption version
Setpoint and Data Memory		32K non-volatile flash RAM
Clock / Calendar		On-board real time clock with battery backup
Environmental Rating		Indoor Type 1
Maximum Cable Length		1000' (300 m)
Warranty		Standard 2 year / Optional 5 year
Weight	Shipping	1 lb (.5 kg)
Dimensions (H $\times$ W $\times$ L)	Shipping	5.75 × 4.25 × 2" (15 × 11 × 5 cm)

Figure 32: OutBack MATE Datasheet

		HUB4	HUB10
Number of Ports		4 Plus MATE	10 Plus MATE
Weight	Unit	1 lb (.5 kg)	1 lb (.5 kg)
	Shipping	3 lbs (1.4 kg)	3 lbs (1.4 kg)
Dimensions (H $\times$ W $\times$ L)	Unit	10.5 × 6.25 × 1.27" (27 × 16 × 3 cm)	$10.5 \times 6.25 \times 1.27$ " (27 × 16 × 3 cm)
	Shipping	$12\times6\times5"~(31\times15\times13~\text{cm})$	$12\times6\times5"~(31\times15\times13~\text{cm})$

Figure 33: OutBack HUB Datasheet

The datasheet for the FlexNET DC is shown in Figure 34 on the next page.

	FN-DC SPECIFICATIONS
Battery Voltage Input Range	8.0 to 80.0 Volts DC
Battery Voltage Resolution	0.1 Volts DC
Number of Current Channels	One to Three (each can be a Source or Load)
Current Range (Each Channel)	-1000.0 Amps to +1000.0 Amps DC
Current Resolution	0.1 Amps DC
State of Charge Display	0 to 100% (1% increments)
Aux Relay Configuration	SPST, Magnetic Latching Relay
Aux Relay Max Rating	5 Amps @ 30 Volts DC
Current Shunt Type (order separately)	500 Amp / 50mv
Display Primary	OutBack Power MATE or MATE2 4 × 20 LCD
Secondary	Five LED Indicators on front of FLEXnet DC
Battery AH Capacity Range	100 to 10,000 Amp Hours
Data Logging Memory	Most recent 128 Days
Programmable AUX Relay Settings Battery Volts	Adjustable from 8.0 to 80.0 VDC
State of Charge	Adjustable from 0 to 100%
Time Delay	Adjustable from 0 to 240 Minutes
Accuracy	0.5% of Reading +/- 2 LSDs per channel
Operating Temperature Range	0 - 50°C
Mounting	3/4" Panel Mount Breaker Slot or Surface Mount
Warranty	Standard 2 year
Weight Unit	5 oz. (.142kg)
Shipping	2 lbs. (.907 kg)
Dimensions (H × W × L Unit	$0.74 \times 3.72 \times 6.60$ " (1.88 $\times$ 9.45 $\times$ 16.75 cm)
Shipping	2.13 × 9 × 11.5" (5.4 × 22.86 × 29.21 cm)

Figure 34: FlexNET DC Datasheet

## **Appendix B.6. Operation and Maintenance Manual**

# **Operation & Maintenance**

# 1. Turning the Lights on/off

- 1.1To turn on the lights,
- 1.2Flip the switch up as shown in figure 1.
- 1.3 Flip the switch down to turn off as shown in figure 2.

**ON** 



Figure 35: Light Switch ON

(http://www.gosolarenergyforlife.com)

**OFF** 



Figure 36: Light switch OFF

 $(http://www.{\tt gosolarenergy for life}.com)$ 



Figure 37: Solar modules

#### 2. Modules

### 2.1 How to measure voltage of a solar module

- **2.1.1** Unplug the panel from the rest of the panels
- 2.1.2 Plug the (+) end of the measuring wire to the (+) terminal of the voltmeter and (-) end into the (-) terminal
- **2.1.3** Make sure the voltmeter is set to measure voltage
- **2.1.4** Clamp the other end of the black wire (-) to the negative (-) terminal of the panels (on the back side), next, clamp the positive end of the red wire to the positive terminal of the panel.
- 2.1.5 Output should now be shown on the voltmeter display

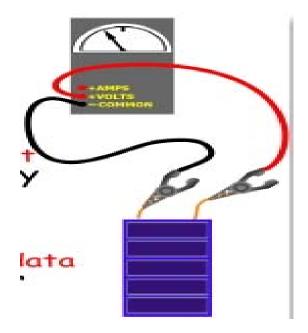


Figure 38: How to measure voltage/current of solar module (http://cleantechnica.com)

# 2.2 Cleaning the Panels

- 2.2.1 Use the soapy water to wash the surface of the solar panels,
- 2.2.2 Brush away any visible dust or streaks. Gentle scrubbing may be necessary as shown in figure 6 below.
- 2.2.3 After wiping away dirt, dry the panels off with a dry towel



Figure 39: cleaning the panels: (http://www.smu.edu)



Figure 40 (http://solarmetalfoil.com/)

### 3. Batteries

#### 3.1 Battery Health

#### 3.1.1 Measuring Voltage of Battery

- 3.1.1.1 Use a voltmeter
- 3.1.1.2 Make sure the batteries are disconnected from the charge controller
- 3.1.1.3 Have the batteries sit for a few hours after disconnecting them from the system

**Take caution!** Batteries are extremely dangerous if improperly handled, installed, or maintained

\*\* Do not short the batteries by connecting the negative and positive terminals of the same battery! This completes the circuit and could result in large spark and could possibly cause a figure, a dangerous electrical shock, and other hazards.



Figure 41 (http://www.sunwindproducts.com)

Shown above in figure 8 is an example of how to measure the voltage of the battery, be sure to connect the red and black terminals to their correct locations on the battery and into the multimeter

## 3.2 Wiring the Batteries

#### 3.2.1 Parallel Connection:

3.2.1.1 Use this to connect two series together by connecting the negative and positive terminals together as shown below at the top and bottom of figure 9.

#### 3.2.2 Series Connection

3.2.2.1.1 Use this to connect batteries together in series by connecting the positive terminals of one battery to the negative thermal of the other. Example is in figure 9 below in the middle wires with red and black ends.

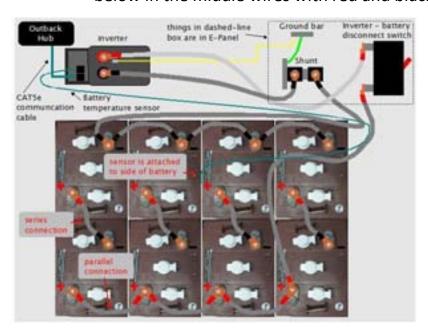


Figure 42: (http://www.sunwindproducts.com)

\*\*Take caution when wiring the batteries\*\*



Figure 43 Figure 44

#### 4. Circuit Breakers:

- 4.1 A Circuit breaker, as shown above in figure 10(many) and 11 (one), is a device designed to open and close a circuit by nonautomatic means and to open the circuit automatically on a predetermined overcurrent without damage to itself when properly applied within its rating. ((NEC))
- 4.2 To open and close a circuit breaker; flip the switch down to close, as they are automatically on the closed (on) position unless something causes them to trip (move to open circuit position).
- 4.3 To turn them on, simply flip the switch to the up position, a sign indicating the on and off position will normally be displayed above and below the switch just in case the on and off positions have been reversed.



Figure 45: two outback inverters (Outbackpower.com)

Inverter DC Breakers

#### 5. Inverters

- 5.1 These inverters are set to be on all the time, the only way to turn them off is to turn off the two main breakers, pointed to in figure 12 above, that take power from the battery.
- 5.2 To cut off the power from the inverters to the loads; turn off the AC breakers located in the AC service panel, which has the (8) AC breakers, and also has (4) other (bigger) AC GFCI breakers.

\*\*Refer to page 6 of the installation manual for more detailed description of the DC side of the inverter and to page 7 for the AC.



Figure 46: outback charge controllers: (Outbackpower.com)

### **6. Charge Controllers**

- 6.1 How to cut off power from the array
  - 6.1.1 Turn the two breakers off that are located on the left side of the main inverter DC breakers.
- 6.2 How to turn them on/off
  - 6.2.1 To turn off: press and hold the power button
  - 6.2.2 To turn on: press the power button

# 7. Trouble Shooting

## 7.1 Common System Faults

#### 7.1.1 These are some of the most common system faults

- Blown Fuses
- ♣ Tripped Breakers
- Bad Connections

### 7.2 Check these before any further actions

- Has the weather been cloudy for several days? If so, system may need recharging
- Check the Array for shading, clean if dirty
- Check system for any loose connections
- 4 Check all fuses and circuit breakers to make sure non of them have tipped

## 7.3 The lights do not turn on

- Check batteries
- Check inverter
- Check circuit breaker (AC)
- Check inverter status

# 7.4 Trouble Shooting Wiring Problems Using a Multimeter

- Measuring AC and DC voltage
- Measuring AC and DC current
- Check the polarity of DC voltage
- > Be sure to acquaint yourself with the volt-ohm-milliamp (VOM) meter. Refer to the operator's manual for proper use of this meter

## 7.5 Measuring Voltage

- 7.5.1 Set the meter to measure DC voltage if measuring voltage/current at any point in the circuit prior to the inverter. Set it to AC voltage if measuring at any point in the circuit after the inverter.
- 7.5.2 Set the range indicator to appropriate scale, if not sure, set it to the highest scale
- Plug the black test lead into the common (-) jack and plug red test lead into the (+) jack as shown in figure 15 below.



Figure 47: using a multimeter: (http://www.ehow.co.uk)

# **7.6.** Troubling Shooting Specific Problems

# 7.6.1. Problem: Load is inoperative

### Possible cause Solutions

Fuse is blown or the circuit breaker	Check fuses and replace if found faulty.
tripped	Check and reset circuit breaker if found
	to have tripped
Circuit open because of break in wire or	Check for continuity of circuit through
there is a loose connection	the load
Appliance has overheat protection	Wait for appliance to cool down and
	reset its thermal protection

# 7.6.2 Battery over/ under charging

### Possible cause Solutions

Controller is not receiver proper battery	Check connections to and from the battery
voltage	Check battery temperature
	Check voltage/current from charge controller
	to battery displayed in the mate
Batteries are too hot	Inspect battery sensor, check for any wire
	damage
	Cut off the power to batteries from charge
	controller and let them cool for a while

# 7.6.3 Charge Controller not operating properly

# Possible cause Solutions

Controller is not receiver proper battery	Check connections to and from the battery
voltage	Check battery temperature
	Check voltage/current from charge controller
	to battery displayed in the mate

Batteries are too hot	Inspect battery sensor, check for any wire
	damage
	Cut off the power to batteries from charge
	controller and let them cool for a while

# 7.6.4 Array Breakers Blows

# Possible cause Solutions

Current through circuit exceeds breaker rating	Let breakers be off for a while, this might be caused by an exceptionally	
	Turn them on again after an hour or two	

## **Appendix C: Other Documentation**

This section shows an updated schedule and budget for the project as well as details on the responsibilities of each team member.

### Appendix C.1. Schedule

The updated schedule for the second semester of the Senior Design Project is shown below in Table 16.

**Table 16: Project Schedule** 

Date	Assignment	Priority
February 15 <sup>th</sup> 2011	Ability to Communicate with MATE using LabVIEW Program	Complete
February 25 <sup>th</sup> 2011	Finalize all Lighting Designs and Photometric Layouts	Complete
March 1 <sup>st</sup> 2011	Finalize all Structural Designs	Complete
March 1 <sup>st</sup> 2011	Finalize Comprehensive Safety Plan	Complete
March 22 <sup>nd</sup> 2011	Complete Skid Construction	Complete
March 24 <sup>th</sup> 2011	Critical Design Review	Complete
March 24 <sup>th</sup> 2011	Critical Design Presentation	Class Requirement
March 29 <sup>th</sup> 2011	Upscale system to include additional Solar Panels	Medium
April 14 <sup>h</sup> 2011	Diagnostics Program Complete	High
April 28 <sup>th</sup> 2011	Full Working Scaled System	High
April 28 <sup>th</sup> 2011	Project Deliverables Complete	High
May 6 <sup>th</sup> 2011	Final Design Report	Class Requirement
May 6 <sup>th</sup> 2011	Spring Engineering Open House	Class Requirement

# Appendix C.2. Budget

An updated budget for the project is shown below in Table 17.

**Table 17: Project Budget** 

Item	Price
RWL-2-1-x4-3L32-HP	\$437.85
EML-4-1x4-4L54	\$338.24
Light Switch	\$23.00
	\$799.09
FlexPower 2-22	\$5,599.95
Remote Temperature Sensor	\$34.94
FlexMax 60 Charge	
Controller	\$530.00
Breaker Panel	\$169.95
5 Piece Outlet Adapter	\$9.99
Standard Outlet	\$3.00
Conduits	\$22.00
14 Gauge Wire	\$14.00
TSM 230 PA05 Solar Panels	\$311.84
Combiner Box	\$126.22
6 Gauge Transmission Wires	\$0.00
AGM Batteries	\$8.93
4/0 Battery Cable	\$190.00
2/0 Battery Cables	\$48.00
MATE	\$222.22
HUB 10	\$281.38
FLEXnet DC	\$275.15
RS232 to USB Cable	\$21.99
LabVIEW	\$0.00
Laptop	\$0.00
80 Amp DC Breaker	\$23.00
120 Amp AC Breaker	\$38.00
Ground Fault Protector	\$113.78
Terminal Bus Bar	\$19.00
Flexware Surge Protector	\$193.73
14 USS Gauge Sheet Metal	\$267.88
3/4" Steel Square Tubing	\$328.53
1.0" Steel Square Tubing	\$596.07
Swivel Wheel Plate Caster	\$54.30
Rigid Wheel Plate Caster	\$44.06
Douglas Fir Green Lumber	\$19.28
Zinc Plated Steel Crown Bolt	\$5.58
Zinc Plated Steel Crown Bolt	\$5.98
Total	\$10,377.84

#### **Appendix C.3. Personnel**

Power Delivery Subsystem (Emmett Perl)

- Integration of all electrical components into the final system
- Programming of the charge controller and inverter for a 48 Volt system
- Wiring of the battery bank (2 parallel connections of 2 batteries)
- Connection from the output of the inverter to the AC service panel
- Wiring of standard type D outlet for the system
- Wiring of light switches/motion sensors wired to control lights
- Programming of LabVIEW to sort data from OutBack MATE
- Design of LabVIEW front panel for power flow program

Mechanical Engineering Subsystem (Enrique Rayon)

- Installation of entire prototype system (responsible for integration of all subsystems)
- Wiring from solar panel location (Loma Hall roof) to demonstration location in Loma 311. Received permission from Dr. Malicky and Dr. McGarry to utilize Loma 311 along with the preexisting wiring from the Wind Turbine on the roof of Loma. Loma 311 will serve as our work room and demonstration room from now until the end of the semester.
- Skid design and construction

After careful consideration and discussion with Dr. McGarry, Dr. Lord and Dr. Pateros the mechanical engineering subsystem deliverable was decided to be an electrical skid. Specifically the subsystem development will involve the design for the skid that will house all the major components of the prototype system excluding the solar panels and combiner box. The skid will house the inverter, charge controller, batteries, diagnostic components (hub, mate, RTS sensor), and lighting fixtures. The skid will have to be a mobile unit that takes into consideration the overheating of electrical equipment in close proximity (thermal readings of all electrical components may be required). In addition the skid will accommodate the wiring/integration needs of the equipment. One of the fundamental design goals of the skid is aesthetics, namely the presentation of all the system components in an organized and easily identifiable manner.

Diagnostic Subsystem (Michael Rios)

- Use LabVIEW to extract data from the OutBack MATE.
- Visual display of system data in both a graphical and text format that can be easily interpreted and understood by someone with no electrical or engineering experience (i.e. a ten year old)
- Battery health and gauge as well as system power flow display.
- Instructions for system debugging in the presence of a system error.
- Error and failure simulations

All interfacing with the customer must be clear and meaningful. The customer needs to be able to quickly, effectively and easily troubleshoot the system failure(s) and or error(s). Ideally the system will diagnose individual component failures (i.e. solar panels and batteries). This may be accomplished with a "smart" system or with a protocol in place that directs the customer to use a Voltmeter or other instrument to test an isolated area.

#### Electrical Safety and Maintenance Subsystem (Mou Riiny)

#### Electrical Safety

- All electrical safety codes will be done according to the NEC
- Conduits will be used to safeguard equipment contact with live wires
- Warning labels will be used where appropriate
- All electrical controls will be housed in a safe, lockable room
- All those who will be maintaining the system will be trained on electrical safety, a manual will be developed to communicate basic electrical safety information
- Ground fault circuit interrupter (GFCI) will be used where there is a lot of human contact

#### Maintenance

- Maintenance for all equipment will be written in a manual
- School administrators will be trained on how to maintain the system
- Equipment that requires more maintenance will be emphasized in manual and training
- Open line of communication will be kept between school administrators and team members
- Extra equipment will be brought in for future replacement if deemed necessary

The deliverable for the safety and maintenance subsystem is training guides/manuals. The goal is to inform the customer in a clear, concise, effective manner. Guides, manuals, presentations, etc. may be used to communicate any necessary information critical to safety and or maintenance. The guides/manuals/presentations will capture a majority if not all of the points listed above under Electrical Safety and Maintenance.